Instabilities of a thin coating on a vertical fibre; Newtonian, shear-thinning, and elastic liquids

Liyan Yu & John Hinch

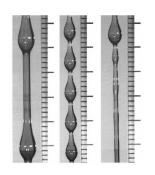
CMS-DAMTP, University of Cambridge

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and Claire McIlroy for elastic liquids

Motivation

Manufacture of polymeric and optical fibres.





Kliakhandler, Davis & Bankoff JFM 2001



Shear-thinning Duprat, Ruyer-Quil & Giorgiutti-Dauphiné

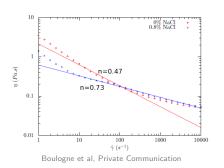
Phys. Fluids 2009

The coating fluid is often non-Newtonian

Constitutive equation

Power-law viscosity:
$$\mu=\beta\left|\frac{\partial u}{\partial y}\right|^{n-1}$$

Xanthan solutions

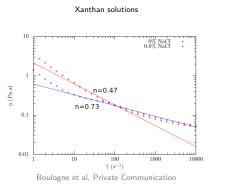


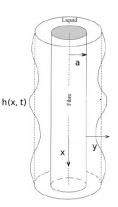
This talk start with power-law, with Newtonian as special case. Elastic at end.

Constitutive equation

Power-law viscosity:
$$\mu = \beta \left| \frac{\partial u}{\partial y} \right|^{n-1}$$

Geometry Axisymmetric





This talk start with power-law, with Newtonian as special case. Elastic at end.

Lubrication framework

Capillary pressure:
$$p = -\gamma \left(\frac{h}{a^2} + h_{xx}\right)$$

Momentum:
$$0 = -\frac{dp}{dx} + \rho g + \frac{\partial \sigma_{xy}}{\partial y}$$

Volume flux:
$$Q = \beta^{-\frac{1}{n}} \frac{n}{2n+1} \left(\rho g - \frac{dp}{dx} \right)^{\frac{1}{n}} h^{(2+\frac{1}{n})}$$

Note:
$$(\cdot)^{\frac{1}{n}} = \operatorname{sign}(\cdot) |\cdot|^{\frac{1}{n}}$$

Mass conservation: $h_t + Q_x = 0$

Non-dimensionalisation

Lengthscales:

- Fibre radius, a, in x direction.
- ▶ Initial film thickness, h_0 , in y direction.

Time:

► Rayleigh instability, $\frac{2n+1}{n} \left(\frac{\beta a^{n+3}}{\gamma h_0^{n+2}} \right)^{\frac{1}{n}}$.

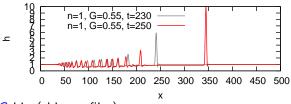
$$h_t + \left(h^{2+\frac{1}{n}}(G + (h+h_{xx})_x)^{\frac{1}{n}}\right)_x = 0$$

where Bond number $G = \frac{\rho g a^3}{\gamma h_0}$.

Time-dependent numerical simulations

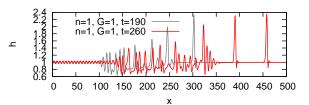
Periodic forcing at inlet: $\omega=1$

G small (thicker film):



Ever growing large pulses

G big (thinner film):



Solitary waves of similar amplitude and speed

This talk: Solitary waves? When? Properties?

Governing equations

In the frame of the solitary waves travelling with speed c:

$$(G + (h + h_{xx})_x) = \frac{\left(c(h-1) + G^{\frac{1}{n}}\right)^n}{h^{2n+1}}$$
 $h \to 1, \quad \text{as} \quad x \to \pm \infty$

Numerically construct the stationary solitary waves.

- ▶ Integrate from $x = -\infty$ to x = 0, and from $x = +\infty$ to x = 0.
- ▶ Hence need starting conditions at $x = \pm \infty$.

Initial conditions for numerics

At
$$x = \pm \infty$$
: $h \sim 1 + \tilde{h}$ with $\tilde{h} \ll 1$.

Linearised equation:

$$\tilde{h}''' + \tilde{h}' - A\tilde{h} = 0$$

where
$$A = nG^{1-1/n}c - (2n+1)G > 0$$
.

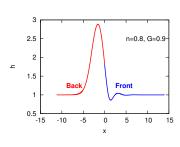
Three solutions of exponential form:

• $h_1 = a_1 e^{m_1 x}$ m_1 real and positive: growing mode.

Use in 'Back' (1 DoF).

 $\tilde{h}_{2,3} = a_{2,3} \mathrm{e}^{m_{2,3} x}$ $m_{2,3}$ complex conjugates with negative real part: decaying modes.

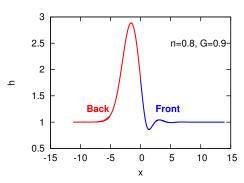
Use in 'Front' (2 DoF).



Numerical construction

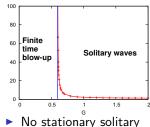
For fixed **G**:

- 1. Shoot from Back, with $a_2 = a_3 = 0$. Stop when h'' = 0, h' < 0.
- 2. Shoot from Front, with $a_1 = 0$. Stop when h'' = 0, h' < 0, h > 1.5.
- 3. Vary the phase of $a_{2,3}$ in Front to match h.
- 4. Vary speed c to match h'.

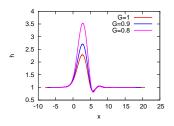


.

Results: n = 1 Kalliadasis & Chang, J. Fluid Mech. 1994



- No stationary solitary waves for G < G₀.</p>
- ▶ As $G \downarrow G_{0+}$, $h_{\text{max}} \rightarrow \infty$.

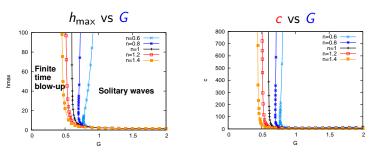


▶ Width of the 'Main Body' independent of G.

Agreement with experiment Quéré, Europhys. Lett. 1990:

- ▶ Critical h_c to observe disturbance $\propto a^3$.

Results: various n (shear-thinning and shear-thickening)



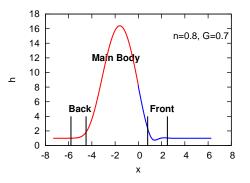
▶ Two branches of solutions for n < 1.

Look at large fast stationary solitary waves close to G_0 .

What determines critical G_0 ? Relationship of h and c with G?

Pulse divided into 3 regions:

- ▶ 'Main body' region: h big, $x \sim O(1)$.
- ▶ 'Front' and 'Back' transition regions: $h \sim O(1)$, x small.



Asymptotic analysis for each region, and match. Very complicated!

Main body region: leading order

h big,
$$x \sim O(1)$$

$$(G + (\mathbf{h} + \mathbf{h}_{xx})_{x}) = \frac{\left(c(h-1) + G^{\frac{1}{n}}\right)^{n}}{h^{2n+1}}$$

Solution: constant capillary pressure $(p = \frac{1}{2}h_{\text{max}})$

$$h = \frac{1}{2}h_{\max}(1-\cos x)$$
 in $0 \le x \le 2\pi$.

For matching,

$$h \sim \frac{1}{4} h_{\text{max}} (x - x_0)^2,$$

with $x_0 = 0$ at the Back and $x_0 = 2\pi$ at the Front.

At leading order main body is at a constant pressure

Transition regions: leading order

 $h \sim O(1)$, x small

$$\left(G+\left(h+\mathbf{h}_{\mathsf{xx}}\right)_{\mathsf{x}}\right)=\frac{\left(c(\mathsf{h}-1)+G^{\frac{1}{n}}\right)^{n}}{\mathsf{h}^{2\mathsf{n}+1}}$$

Transition regions: $x \sim c^{-n/3}$.

Modified Bretherton equation:

$$h_{\xi\xi\xi}=rac{(h-1)^n}{h^{2n+1}}$$
 with $\xi=c^{n/3}(x-x_0).$ $(x_0=0 ext{ at 'Back' and } x_0=2\pi ext{ at 'Front'.})$

Transition regions: leading order

$$h \sim O(1)$$
, x small

$$(G + (h + \mathbf{h}_{xx})_{x}) = \frac{\left(c(\mathbf{h} - 1) + G^{\frac{1}{n}}\right)^{n}}{\mathbf{h}^{2n+1}}$$

Transition regions: $x \sim c^{-n/3}$.

Modified Bretherton equation:

$$h_{\xi\xi\xi}=rac{(h-1)^n}{h^{2n+1}}$$
 with $\xi=c^{n/3}(x-x_0).$ $(x_0=0 ext{ at 'Back' and } x_0=2\pi ext{ at 'Front'.})$

For matching, solutions towards 'Main Body' (h becoming large)

$$h \sim \frac{1}{2}P_{\pm}\xi^2 + Q\xi + R_{\pm}$$
 as $\xi \to \pm \infty$

Use 1 DoF to redefine origin so Q = 0.

Matching: leading order

DoFs at Back: 1-1(Q=0)=0. P_+ and R_+ uniquely determined. DoFs at Front: 2-1(Q=0)=1. One parameter in P_- and R_- .

Main body: $h \sim \frac{1}{4} h_{\text{max}} (x - x_0)^2$ near $x_0 = 0, 2\pi$.

Transition regions: $h \sim \frac{1}{2}P_{\pm}\xi^2 + R_{\pm}$ as $\xi \to \pm \infty$.

Matching, i.e. same quadratic:

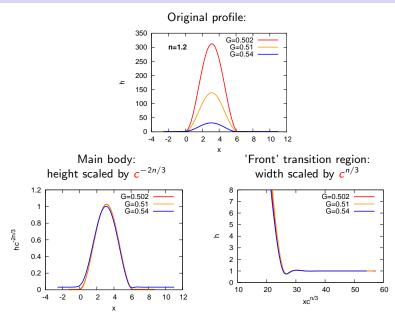
$$P_{-} = P_{+}$$

So now P_{-} unique and hence R_{-} unique.

$$\frac{1}{2}P(\xi = c^{n/3}(x - x_0))^2 = \frac{1}{4}h_{\text{max}}(x - x_0)^2$$
$$h_{\text{max}} = 2Pc^{2n/3}$$

Note: capillary pressure in the main body $p = \frac{1}{2}h_{max} = Pc^{2n/3}$.

Checking scalings



So far have $h_{\text{max}}(c)$. G yet to appear

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Transition regions: $h \sim \frac{1}{2}P\xi^2 + R_{\pm}$.

▶ Different apparent film thickness, R_{\pm} , at 'Back' and 'Front'.

Need 1st correction of Main Body:
$$h \sim c^{2n/3}h_0 + h_2$$

$$(\mathbf{G} + (\mathbf{h} + \mathbf{h}_{xx})_{x}) = \frac{\left(\mathbf{c}(h-1) + \mathbf{G}^{\frac{1}{n}}\right)^{n}}{h^{2n+1}}$$

$$\mathbf{G}_{0} + (h_{2} + h_{2xx})_{x} = 0$$

So far have $h_{\text{max}}(c)$. G yet to appear

Transition regions: $h \sim \frac{1}{2}P\xi^2 + R_{\pm}$.

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Need 1st correction of Main Body: $h \sim c^{2n/3}h_0 + h_2$

$$(\mathbf{G} + (\mathbf{h} + \mathbf{h_{xx}})_{\mathbf{x}}) = \frac{\left(c(h-1) + G^{\frac{1}{n}}\right)^n}{h^{2n+1}}$$

$$G_0 + (h_2 + h_{2xx})_x = 0$$

Solution (hydrostatic pressure gradient):

$$h_2 = -G_0(x - \sin x) + R_+$$
 in $0 \le x \le 2\pi$.

Matching gives critical G_0 :

$$G_0 = (R_+ - R_-)/2\pi$$

 $2\pi G_0$ pressure difference between pushing and pulling transitions

c as a function of G

So far have $h_{\text{max}}(c)$ and critical G_0 . Yet to find G(c).

c as a function of G

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Need 2nd correction in Main Body:

$$h \sim c^{2n/3}h_0 + h_2 + c^{-(2n-1)n/3}h_3$$

$$G = G_0 + c^{-(2n-1)n/3}G_1$$

$$(h_3 + h_{3xx})_x = \left(\frac{1}{P^{n+1}(1-\cos x)^{n+1}} - G_1\right)$$

Solution

$$\begin{split} P^{n+1}h_3 &= \frac{(n+1)\sin x}{n(2n+1)(1-\cos x)^n} - \frac{(n+(n+1)\cos x)\sin x}{(2n+1)(2n-1)(1-\cos x)^n} \\ &\quad + \frac{(n-1)(n+(n+1)\cos x)}{(2n+1)(2n-1)} \int_{\pi}^{x} \frac{1}{(1-\cos t)^{n-1}} \, dt - G_1 x \end{split}$$

c as a function of G

Near $x = x_0$

$$h_3 \sim S(x-x_0)^{1-2n} + D_{\pm} - G_1 x + \dots$$

- ▶ The singular term matches the same in transition regions.
- ▶ D+ different at the 'Back' and 'Front'.
- ▶ No terms to match with them from transition regions.
- ▶ Hence need:

$$G_1 = (D_+ - D_-)/2\pi$$

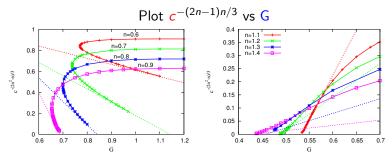
Finally we have found the relationship between c and G

$$G = G_0 + c^{-(2n-1)n/3}G_1$$

 $2\pi G_1$ is the extra pressure difference compared with n=1 to drive flow through main body

Results

$$G = G_0 + c^{-(2n-1)n/3}G_1$$



- ▶ When n < 1, $G_1 < 0$. Negative slope at G_0 .
- ▶ When n > 1, $G_1 > 0$. Positive slope at G_0 .
- ▶ When n = 1, $G_1 = 0$. No relationship between G and C yet.

transition regions

With scaling $\xi = c^{n/3}(x - x_0)$,

$$h_{\xi\xi\xi} = \frac{(h-1)^n}{h^{2n+1}} - c^{-2n/3}h_{\xi} - c^{-n}G + c^{-1}\frac{n(h-1)^{n-1}G^{1/n}}{h^{2n+1}} + \dots$$

Expand h as

$$h \sim h_0 + c^{-2n/3}h_2 + c^{-n}h_3 + c^{-1}h_4 + c^{-4n/3}h_5 + \dots$$

$$\begin{split} h_0^{\prime\prime\prime} &= \frac{(h-1)^n}{h^{2n+1}}, & h_0 \sim \frac{P}{2} \xi^2 + R_\pm + 5 x^{1-2n} \\ h_2^{\prime\prime\prime} &= \frac{(h_0-1)^{n-1} \left(-(n+1)h_0 + (2n+1) \right)}{h_0^{2n+2}} h_2 - h_0^\prime, & h_2 \sim -\frac{P}{4!} \xi^4 + \frac{a_{2\pm}}{2} \xi^2 + c_{2\pm} + k_2 \xi^{3-2n} \\ h_3^{\prime\prime\prime} &= \frac{(h_0-1)^{n-1} \left(-(n+1)h_0 + (2n+1) \right)}{h_0^{2n+2}} h_3 - G_0, & h_3 \sim -\frac{G_0}{3!} \xi^3 + \frac{a_{3\pm}}{2} \xi^2 + c_{3\pm} \\ h_4^{\prime\prime\prime} &= \frac{(h_0-1)^{n-1} \left(-(n+1)h_0 + (2n+1) \right)}{h_0^{2n+2}} h_4 & h_4 \sim \frac{1}{2} a_{4\pm} \xi^2 + c_{4\pm} \\ &+ \frac{n(h_0-1)^{n-1} G_0^{1/n}}{h_0^{2n+1}}, \end{split}$$

main body

With
$$h = c^{2n/3}H$$
,

$$(H+H_{xx})_x = -c^{-2n/3}G + c^{-(2n+1)n/3}\frac{\left(1 - \frac{c^{-2n/3}}{H} + \frac{G^{1/n}(c^{-1-2n/3})}{H}\right)^n}{H^{n+1}}.$$

Expand H as

$$H \sim H_0 + c^{-2n/3}H_2 + c^{-(2n+1)n/3}H_3 + c^{-n}H_4 + c^{-1}H_5 + c^{-4n/3}H_6 + \dots$$

and G as

$$G \sim G_0 + G_1 c^{-(2n-1)n/3} + G_2 c^{-2n/3} + \dots$$

$$\begin{split} H_0' &+ H_0''' &= 0, \\ H_2' &+ H_2''' &= -G_0 \\ H_3' &+ H_3''' &= -G_1 + \frac{1}{P^{n+1}(1-\cos x)^{n+1}}, \\ H_4' &+ H_4''' &= 0, \\ H_5' &+ H_5''' &= 0, \\ H_6' &+ H_6''' &= -G_2, \end{split} \qquad \begin{split} H_0 &= P(1-\cos x) \\ H_2 &= G_0 \left(\sin x - x\right) + A_2 + C_2 \cos x \\ H_2 &= G_0 \left(\sin x - x\right) + A_2 + C_2 \cos x \\ H_3 &\sim Sx^{1-2n} + D_{\pm} - G_1x + k_2x^{3-2n} \\ H_4 &= A_4 + B_4 \sin x + C_4 \cos x \\ H_5 &= A_5 + B_5 \sin x + C_5 \cos x \\ H_6' &= G_2 \left(\sin x - x\right) + A_6 + B_6 \sin x + C_6 \cos x \end{split}$$

Matching: transition regions

Transition regions=

Matching: main body region

Main body=

$$c^{\frac{2n}{3}} \quad \left[\frac{P}{2}x^2 - \frac{P}{4!}x^4 + \frac{P}{6!}x^6 + \dots \right]$$

$$+c^0 \quad \left[-G_0x_0 + A_2 + C_2 - \frac{C_2}{2}x^2 - \frac{G_0}{3!}x^3 + \frac{C_2}{4!}x^4 + \dots \right]$$

$$+c^{-\frac{2n^2}{3} + \frac{n}{3}} \quad \left[Sx^{1-2n} - G_1x_0 + D_{\pm} + k_2x^{3-2n} + k_3x^{5-2n} + \dots \right]$$

$$+c^{-\frac{n}{3}} \quad \left[A_4 + C_4 - \frac{C_4}{2}x^2 + \dots \right]$$

$$+c^{\frac{2n}{3} - 1} \quad \left[A_5 + C_5 - \frac{C_5}{2}x^2 \right]$$

$$+c^{-\frac{2n}{3}} \quad \left[-G_2x_0 + A_6 + C_6 - \frac{C_6}{2}x^2 - \frac{G_2 + B_6}{3!}x^3 + \dots \right]$$

More terms: matching two regions

Hence,

At
$$c^0$$
:
$$G_0=(R_+-R_-)/2\pi$$
 At $c^{-(2n^2-n)/3}$:
$$G_1=-(D_+-D_-)/2\pi$$
 At c^{-1} :
$$G_2=(c_{2+}-c_{2-})/2\pi$$

 $G = G_0 + G_1 c^{-(2n-1)n/3} + G_2 c^{-2n/3}$

More terms: Results

$$G = G_0 + G_1 c^{-(2n-1)n/3} + G_2 c^{-2n/3}$$

Plot **G** vs
$$c^{-(2n-1)n/3}$$

$$n = 0.9 \qquad \qquad n = 1.2$$

Small improvement by second correction to *G*

More terms: Results

$$G = G_0 + G_1 c^{-(2n^2-n)/3} + G_2 c^{-2n/3}$$

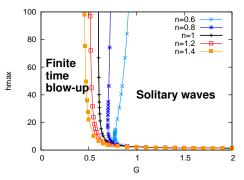
When n = 1, $G_1 = 0$, so

$$G = G_0 + G_2 c^{-2/3}$$

Need even more terms for Newtonian n = 1 – see beyond end.

 $2\pi G_2$ comes from corrections in the transition regions due to the small axial curvature

Two branches for n < 1



Upper branch is unstable – solutions either blow up or decay to lower branch.

Hence there is a maximum size of stable solitary for shear-thinning fluids.

Summarising

Main Body at constant pressure $h \sim c^{2n/3}P(1-\cos x)$.

Cause of all difficulty: length 2π not changing.

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 $2\pi G_0$ is extra hydrostatic pressure difference needed to push front transisiton region compared with pulling rear one.

Three mechanisms determine how c depends on $G - G_0$:

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Main Body at constant pressure $h \sim c^{2n/3}P(1-\cos x)$.

Cause of all difficulty: length 2π not changing.

 $2\pi G_0$ is extra hydrostatic pressure difference needed to push front transisiton region compared with pulling rear one.

Three mechanisms determine how c depends on $G - G_0$:

- For power-law fluids, $G G_0 \sim G_1 c^{-(2n-1)n/3}$ for pressure to drive flow though main body,
- For Newtonian (n=1) fluids, $G G_0 \sim G_2 c^{-2/3}$ effect of axial capillary pressure in the transition regions,
- For large amplitudes comparable with fibre radius, $G G_0 \sim -\mathrm{amp} c^{-2/3} 3PG_0$ because pendant drop is longer.

Symmetry breaking instability with elastic liquids with Claire McIlroy

- François Boulogne observed in his Paris PhD thesis that the coating of an elastic liquid was never axisymmetric, but was always thicker on one side.
- Flow in thin coating is mainly simple shear and quasi-steady (varies over distances much greater than thickness).
- ▶ Hence rheology is a viscosity plus normal stresses.
- ► First normal stress difference = tension in streamlines → enhanced effective surface tension.
- \blacktriangleright Second normal stress difference = tension in vortex lines \rightarrow new instability.

Governing equation

Extra non-Newtonian stress for a second-order fluid

$$\sigma^{NN} = -2\alpha \stackrel{\nabla}{E} + \beta E^2,$$

 α tension in the streamlines, $\beta < 0$ tension in the vortex lines.

$$\frac{\partial h}{\partial t} + G \frac{\partial h^3}{\partial z} + \nabla h^3 \nabla (h + \nabla^2 h) + A \frac{\partial^2}{\partial z^2} h^5 + B \frac{\partial^2}{\partial \theta^2} h^5 = 0,$$

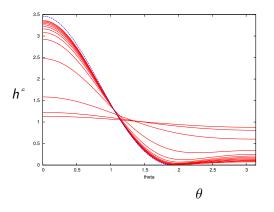
(curiously
$$A \sim \alpha/6$$
, but $B \sim -\beta/80$)

Now study development of lop-sided flow with $h(\theta, t)$, no z-variations.

$$h_t + \left(h^3(h_{\theta\theta} + h + Bh^2)_{\theta}\right)_{\theta} = 0$$

Time evolution

$$h(\theta, t)$$
 at $t = 2^n$ $n = -2, ..., 11$, for $B = 0.5$.

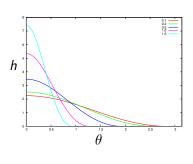


Dotted blue is a steady state which wets only $0 \le \theta \le 1.9071$

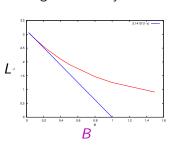
(Interesting intermediate times: drift of an off-centred cylinder.)

Symmetry breaking instability with elastic liquids Steady states

Steady states for various B

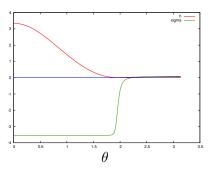


Length of steady state



Structure at late times

The shape and the pressure (stress $\sigma_{\theta\theta}$) at $t=10^3$ for B=0.5

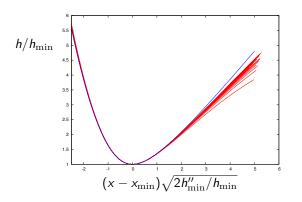


There two constant pressure regions.

Higher pressure region to the right drains into the lower pressure region to the left through a small neck.

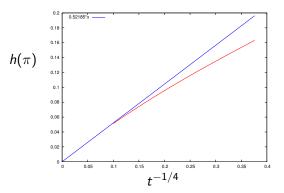
The neck between the two constant pressure regions

Universal shape of the neck between the two constant pressure regions, for $t = 50 (50) 10^3$ and for B = 0.5.



Blue shape from Bretherton's equation.

Draining of small region



$$h(\pi) = \frac{1 + \cos L}{t^{1/4}} \left(\frac{K((\pi - L)\cos L + \sin L)}{4Q\sin^5 L} \right)^{1/4}$$

with Bretherton Q=1.20936 and for B=0.5 pressure in steady state K=3.7297 and length of steady state L=1.9171.

Future Work

- ► Normal stress effect. √
- ▶ Relax the thin film approximation? √
- Newtonian fluid n=1 $\sqrt{}$
- ▶ What happens at big G? √
- ► Finite flow domain for shear-thinning fluids √
- Comparison with experimental data.

n = 1 Newtonian fluid, even more terms

Matching: transition regions

Transition regions=

n = 1 Newtonian fluid, even more terms

Matching: main body region

$$\mathsf{Main}\ \mathsf{body} =$$

$$c^{2/3} \quad \left[\frac{P}{2} x^2 - \frac{P}{4!} x^4 + \frac{P}{6!} x^6 + \dots \right]$$

$$+c^0 \quad \left[-G_0 x_0 + A_2 + C_2 - \frac{C_2}{2} x^2 - \frac{G_0}{3!} x^3 + \frac{C_2}{4!} x^4 + \dots \right]$$

$$+c^{-1/3} \quad \left[-\frac{2}{3P^2 x} + (A_3 + C_3) + (\frac{1}{18P^2} + B_3) x - \frac{C_3}{2} x^2 + (\frac{1}{1080P^2} - \frac{B_3}{3!}) x^3 + \dots \right]$$

$$+c^{-2/3} \quad \left[-G_2 x_0 + A_4 + C_4 + B_4 x - \frac{C_4}{2} x^2 - \frac{G_2}{3!} x^3 + \dots \right]$$

$$+c^{-1} \log c \quad \left[A_5 + C_5 - \frac{C_5}{2} x^2 + \dots \right]$$

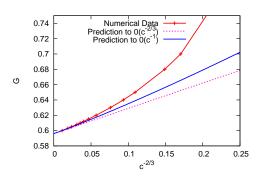
$$+c^{-1} \quad \left[\frac{2(1+2R_{\pm})}{150^3 x^3} + \frac{4(1+2A_2-3C_2)}{150^3 x^3} + \frac{4G_0}{2P^3} \log x - G_3 x_0 + A_6 + C_6 \dots \right]$$

n = 1 Newtonian fluid, even more terms

Results

At
$$c^0$$
: $G_0 = (R_+ - R_-)/2\pi$
At $c^{-2/3}$: $G_2 = (c_{2+} - c_{2-})/2\pi$
At c^{-1} : $G_3 = (c_{3+} - c_{3-})/2\pi$
Hence,

$$G = G_0 + G_2 c^{-2/3} + G_3 c^{-1}$$



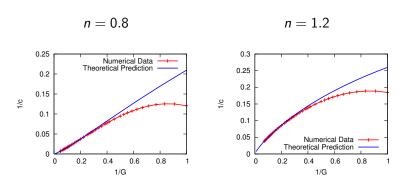
$$h \sim 1 + \frac{1}{G}h_1$$
 $c \sim \left(2 + \frac{1}{n}\right)G^{\frac{1}{n}} + c_1G^{\frac{1}{n}-1}$

where h_1 satisfies the nonlinear equation

$$h_1' + h_1''' = nc_1h_1 + h_1^2\left(-n(2n+1) + \frac{n(n-1)}{2}\left(2 + \frac{1}{n}\right)^2\right)$$

This equation can be solved numerically to give the value of c_1 for different values of n.

Big G results



Finite flow domain for shear-thinning fluids

Modified Bretherton equation

$$h'''=\frac{(h-1)^n}{h^{2n+1}}$$

Integrating from $\pm \infty$ where $h \sim 1 + \tilde{h}$ ($\tilde{h} \ll 1$), \tilde{h} satisfies:

$$\tilde{h}''' = \tilde{h}^n$$
. \Leftarrow No exponential solutions for $n \neq 1$.

Solution at 'Back'

$$\tilde{h} = A(\xi - \xi_0)^{\frac{3}{1-n}}, \quad n < 1$$

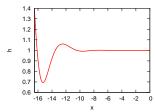
 \tilde{h} becomes 0 at a finite distance.

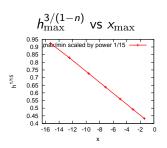
While viscosity thins as $\gamma \to \infty$ it thickens as $\gamma \to 0$, and so flow stops in a finite distance.

Finite flow domain for shear-thinning fluids

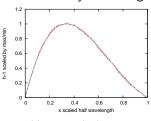
Solution at 'Front' (n = 0.8)

Decaying nonlinear oscillations





Each half-cycle normalised by maximum and by wavelength



Universal shape

Decays to zero in finite distance