

Resumé of lecture 2

Driven Cavity in ψ - ω formulation.

Finite Differences

Poisson problem. SOR.

Test against theoretical solution: $O(\Delta x^2)$ error?

2.7 Vorticity evolution

$$\frac{\partial \omega}{\partial t} = -\frac{\partial(\omega, \psi)}{\partial(x, y)} + \frac{1}{Re} \nabla^2 \omega$$

with $\omega = 0$ at $t = 0$.

2.7 Vorticity evolution

$$\frac{\partial \omega}{\partial t} = -\frac{\partial(\omega, \psi)}{\partial(x, y)} + \frac{1}{Re} \nabla^2 \omega$$

with $\omega = 0$ at $t = 0$.

Forward time-step from $t = n\Delta t$ to $t = (n + 1)\Delta t$
at interior points $i = 1 \rightarrow N - 1, j = 1 \rightarrow N - 1$

2.7 Vorticity evolution

$$\frac{\partial \omega}{\partial t} = -\frac{\partial(\omega, \psi)}{\partial(x, y)} + \frac{1}{Re} \nabla^2 \omega$$

with $\omega = 0$ at $t = 0$.

Forward time-step from $t = n\Delta t$ to $t = (n+1)\Delta t$
at interior points $i = 1 \rightarrow N-1$, $j = 1 \rightarrow N-1$

$$\omega_{ij}^{n+1} = \omega_{ij}^n + \Delta t \left[-\frac{\psi_{ij+1}^n - \psi_{ij-1}^n}{2\Delta x} \frac{\omega_{i+1j}^n - \omega_{i-1j}^n}{2\Delta x} + \frac{\psi_{i+1j}^n - \psi_{i-1j}^n}{2\Delta x} \frac{\omega_{ij+1}^n - \omega_{ij-1}^n}{2\Delta x} \right] + \frac{\Delta t}{Re\Delta x^2} \begin{pmatrix} 1 & 1 & 1 \\ 1 & -4 & 1 \\ 1 & 1 & 1 \end{pmatrix} \omega_{ij}^n$$

2.7 Vorticity evolution

$$\frac{\partial \omega}{\partial t} = -\frac{\partial(\omega, \psi)}{\partial(x, y)} + \frac{1}{Re} \nabla^2 \omega$$

with $\omega = 0$ at $t = 0$.

Forward time-step from $t = n\Delta t$ to $t = (n+1)\Delta t$
at interior points $i = 1 \rightarrow N-1, j = 1 \rightarrow N-1$

$$\omega_{ij}^{n+1} = \omega_{ij}^n + \Delta t \left[-\frac{\psi_{ij+1}^n - \psi_{ij-1}^n}{2\Delta x} \frac{\omega_{i+1j}^n - \omega_{i-1j}^n}{2\Delta x} + \frac{\psi_{i+1j}^n - \psi_{i-1j}^n}{2\Delta x} \frac{\omega_{ij+1}^n - \omega_{ij-1}^n}{2\Delta x} \right] + \frac{\Delta t}{Re\Delta x^2} \begin{pmatrix} 1 & 1 & 1 \\ 1 & -4 & 1 \\ 1 & 1 & 1 \end{pmatrix} \omega_{ij}^n$$

On boundary need $\psi = 0$, and value of ω

Boundary condition on ω – so that $\frac{\partial \psi}{\partial n} = U_{\text{wall}}$

Boundary condition on ω – so that $\frac{\partial\psi}{\partial n} = U_{\text{wall}}$

For bottom $y = 0$:

$$u_{\frac{1}{2}} = \frac{\psi_{i1} - \psi_{i0}}{\Delta x}$$

Boundary condition on ω – so that $\frac{\partial \psi}{\partial n} = U_{\text{wall}}$

For bottom $y = 0$:

$$u_{\frac{1}{2}} = \frac{\psi_{i1} - \psi_{i0}}{\Delta x}$$

so

$$\omega_{\frac{1}{4}} = \frac{u_{\frac{1}{2}} - U_{\text{wall}}}{\frac{1}{2}\Delta x}$$

Boundary condition on ω – so that $\frac{\partial \psi}{\partial n} = U_{\text{wall}}$

For bottom $y = 0$:

$$u_{\frac{1}{2}} = \frac{\psi_{i1} - \psi_{i0}}{\Delta x}$$

so

$$\omega_{\frac{1}{4}} = \frac{u_{\frac{1}{2}} - U_{\text{wall}}}{\frac{1}{2}\Delta x}$$

1st order BC

$$\omega_0 \approx \omega_{\frac{1}{4}} = \frac{\frac{\psi_{i1} - \psi_{i0}}{\Delta x} - U_{\text{wall}}}{\frac{1}{2}\Delta x}$$

Boundary condition on ω – so that $\frac{\partial \psi}{\partial n} = U_{\text{wall}}$

For bottom $y = 0$:

$$u_{\frac{1}{2}} = \frac{\psi_{i1} - \psi_{i0}}{\Delta x}$$

so

$$\omega_{\frac{1}{4}} = \frac{u_{\frac{1}{2}} - U_{\text{wall}}}{\frac{1}{2}\Delta x}$$

1st order BC

$$\omega_0 \approx \omega_{\frac{1}{4}} = \frac{\frac{\psi_{i1} - \psi_{i0}}{\Delta x} - U_{\text{wall}}}{\frac{1}{2}\Delta x}$$

2nd order, by linear extrapolation

$$\omega_0 \approx \frac{4\omega_{\frac{1}{4}} - \omega_1}{3}.$$

Boundary condition on ω – so that $\frac{\partial \psi}{\partial n} = U_{\text{wall}}$

For bottom $y = 0$:

$$u_{\frac{1}{2}} = \frac{\psi_{i1} - \psi_{i0}}{\Delta x}$$

so

$$\omega_{\frac{1}{4}} = \frac{u_{\frac{1}{2}} - U_{\text{wall}}}{\frac{1}{2}\Delta x}$$

1st order BC

$$\omega_0 \approx \omega_{\frac{1}{4}} = \frac{\frac{\psi_{i1} - \psi_{i0}}{\Delta x} - U_{\text{wall}}}{\frac{1}{2}\Delta x}$$

2nd order, by linear extrapolation

$$\omega_0 \approx \frac{4\omega_{\frac{1}{4}} - \omega_1}{3}.$$

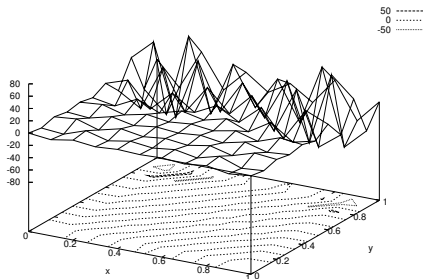
Starts at $t = 0$ as numerical delta function, then diffuses.

2.8 Time-step instability

plot ω for $Re = 10$ at $t = 0.525$ with $\Delta t = 0.035$ and $\Delta x = 0.1$

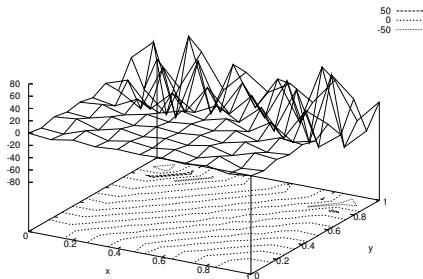
2.8 Time-step instability

plot ω for $Re = 10$ at $t = 0.525$ with $\Delta t = 0.035$ and $\Delta x = 0.1$



2.8 Time-step instability

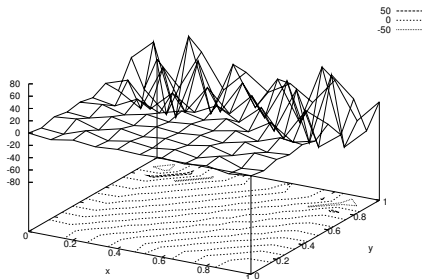
plot ω for $Re = 10$ at $t = 0.525$ with $\Delta t = 0.035$ and $\Delta x = 0.1$



Numerical or physical instability?

2.8 Time-step instability

plot ω for $Re = 10$ at $t = 0.525$ with $\Delta t = 0.035$ and $\Delta x = 0.1$



Numerical or physical instability?

Not physically unstable at $Re = 10$ surely?

Time step instability 2

Checker board pattern.

+	-	+
-	+	-
+	-	+

Time step instability 2

Checker board pattern.

+	-	+
-	+	-
+	-	+

$$\omega_{ij}^n = (-)^{i+j} A_n,$$

Time step instability 2

Checker board pattern.

+	-	+
-	+	-
+	-	+

$$\omega_{ij}^n = (-)^{i+j} A_n,$$

Diffusion terms in time-stepping algorithm

Time step instability 2

Checker board pattern.

+	-	+
-	+	-
+	-	+

$$\omega_{ij}^n = (-)^{i+j} A_n,$$

Diffusion terms in time-stepping algorithm

$$A_{n+1} = A_n + \frac{\Delta t}{Re\Delta x^2} \cdot -8A_n$$

Time step instability 2

Checker board pattern.

+	-	+
-	+	-
+	-	+

$$\omega_{ij}^n = (-)^{i+j} A_n,$$

Diffusion terms in time-stepping algorithm

$$A_{n+1} = A_n + \frac{\Delta t}{Re\Delta x^2} \cdot -8A_n$$

Stable if $\Delta t < \frac{1}{4} Re\Delta x^2$

Time step instability 2

Checker board pattern.

+	-	+
-	+	-
+	-	+

$$\omega_{ij}^n = (-)^{i+j} A_n,$$

Diffusion terms in time-stepping algorithm

$$A_{n+1} = A_n + \frac{\Delta t}{Re\Delta x^2} \cdot -8A_n$$

Stable if $\Delta t < \frac{1}{4} Re\Delta x^2$ – at least one Δt to diffuse one Δx .

Time step instability 2

Checker board pattern.

+	-	+
-	+	-
+	-	+

$$\omega_{ij}^n = (-)^{i+j} A_n,$$

Diffusion terms in time-stepping algorithm

$$A_{n+1} = A_n + \frac{\Delta t}{Re\Delta x^2} \cdot -8A_n$$

Stable if $\Delta t < \frac{1}{4} Re\Delta x^2$ – at least one Δt to diffuse one Δx .

EJH works at $\frac{1}{5}$.

Advection instability \rightarrow CFL condition

(Courant-Friedricks-Lewy)

Stable if $\Delta t < \Delta x / U_{\max}$

Advection instability \rightarrow CFL condition

(Courant-Friedricks-Lewy)

Stable if $\Delta t < \Delta x / U_{\max}$ – at least one Δt to advect one Δx .

Advection instability \rightarrow CFL condition

(Courant-Friedricks-Lewy)

Stable if $\Delta t < \Delta x / U_{\max}$ – at least one Δt to advect one Δx .

Must resolve boundary layers

Advection instability \rightarrow CFL condition

(Courant-Friedricks-Lewy)

Stable if $\Delta t < \Delta x / U_{\max}$ – at least one Δt to advect one Δx .

Must resolve boundary layers

Dimensional: $U_{\max} \Delta x / \nu < 1 \Leftrightarrow$

Advection instability \rightarrow CFL condition

(Courant-Friedricks-Lewy)

Stable if $\Delta t < \Delta x / U_{\max}$ – at least one Δt to advect one Δx .

Must resolve boundary layers

Dimensional: $U_{\max} \Delta x / \nu < 1 \Leftrightarrow$ Nondimensional $\Delta x < \frac{1}{Re}$.

Advection instability \rightarrow CFL condition

(Courant-Friedricks-Lewy)

Stable if $\Delta t < \Delta x / U_{\max}$ – at least one Δt to advect one Δx .

Must resolve boundary layers

Dimensional: $U_{\max} \Delta x / \nu < 1 \Leftrightarrow$ Nondimensional $\Delta x < \frac{1}{Re}$.

This + stable diffusion \Rightarrow stable advection

Advection instability \rightarrow CFL condition

(Courant-Friedricks-Lewy)

Stable if $\Delta t < \Delta x / U_{\max}$ – at least one Δt to advect one Δx .

Must resolve boundary layers

Dimensional: $U_{\max} \Delta x / \nu < 1 \Leftrightarrow$ Nondimensional $\Delta x < \frac{1}{Re}$.

This + stable diffusion \Rightarrow stable advection

Total cost to $t = 1$

Advection instability \rightarrow CFL condition

(Courant-Friedricks-Lewy)

Stable if $\Delta t < \Delta x / U_{\max}$ – at least one Δt to advect one Δx .

Must resolve boundary layers

Dimensional: $U_{\max} \Delta x / \nu < 1 \Leftrightarrow$ Nondimensional $\Delta x < \frac{1}{Re}$.

This + stable diffusion \Rightarrow stable advection

Total cost to $t = 1$

$$\left(\# \text{ time steps } \frac{1}{\Delta t} \propto N^2 \right) \times$$

Advection instability \rightarrow CFL condition

(Courant-Friedricks-Lewy)

Stable if $\Delta t < \Delta x / U_{\max}$ – at least one Δt to advect one Δx .

Must resolve boundary layers

Dimensional: $U_{\max} \Delta x / \nu < 1 \Leftrightarrow$ Nondimensional $\Delta x < \frac{1}{Re}$.

This + stable diffusion \Rightarrow stable advection

Total cost to $t = 1$

$$\left(\# \text{ time steps } \frac{1}{\Delta t} \propto N^2 \right) \times (\text{cost per time step (SOR)} \propto N^3)$$

Advection instability \rightarrow CFL condition

(Courant-Friedricks-Lewy)

Stable if $\Delta t < \Delta x / U_{\max}$ – at least one Δt to advect one Δx .

Must resolve boundary layers

Dimensional: $U_{\max} \Delta x / \nu < 1 \Leftrightarrow$ Nondimensional $\Delta x < \frac{1}{Re}$.

This + stable diffusion \Rightarrow stable advection

Total cost to $t = 1$

$$\left(\# \text{ time steps } \frac{1}{\Delta t} \propto N^2 \right) \times \left(\text{cost per time step (SOR)} \propto N^3 \right) \\ \propto N^5$$

Hence doubling N is 32 times longer, quadruple N is 1024 longer.

Advection instability \rightarrow CFL condition

(Courant-Friedricks-Lewy)

Stable if $\Delta t < \Delta x / U_{\max}$ – at least one Δt to advect one Δx .

Must resolve boundary layers

Dimensional: $U_{\max} \Delta x / \nu < 1 \Leftrightarrow$ Nondimensional $\Delta x < \frac{1}{Re}$.

This + stable diffusion \Rightarrow stable advection

Total cost to $t = 1$

$$\left(\# \text{ time steps } \frac{1}{\Delta t} \propto N^2 \right) \times \left(\text{cost per time step (SOR)} \propto N^3 \right) \\ \propto N^5$$

Hence doubling N is 32 times longer, quadruple N is 1024 longer.

'Better' time step algorithms \rightarrow larger Δt , but more accurate?

2.9 Accuracy consistency. a. Time-stepping

No analytic solution to test

2.9 Accuracy consistency. a. Time-stepping

No analytic solution to test \rightarrow test code has designed accuracy $O(\Delta t, \Delta x^2)$.

2.9 Accuracy consistency. a. Time-stepping

No analytic solution to test \rightarrow test code has designed accuracy $O(\Delta t, \Delta x^2)$.

Forward differencing $\rightarrow O(\Delta t)$ errors.

2.9 Accuracy consistency. a. Time-stepping

No analytic solution to test \rightarrow test code has designed accuracy $O(\Delta t, \Delta x^2)$.

Forward differencing $\rightarrow O(\Delta t)$ errors.

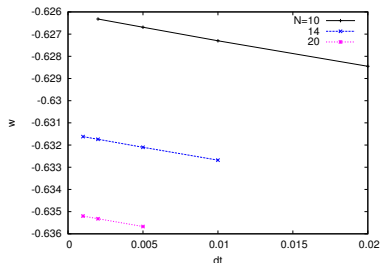
Look at $\omega(x = 0.5, y = 0.5, t = 1)$ – **exactly** (0.5, 0.5, 1)

2.9 Accuracy consistency. a. Time-stepping

No analytic solution to test \rightarrow test code has designed accuracy $O(\Delta t, \Delta x^2)$.

Forward differencing $\rightarrow O(\Delta t)$ errors.

Look at $\omega(x = 0.5, y = 0.5, t = 1)$ – **exactly** (0.5, 0.5, 1)
1st order BC for ω_0 with $Re = 10$ and $N = 10, 14$ and 20 .



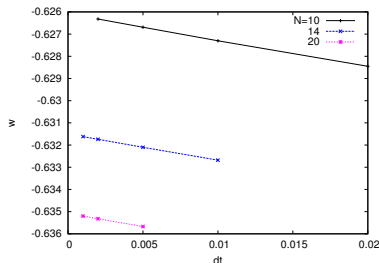
Note: linear in Δt , very very small Δt (larger unstable),

2.9 Accuracy consistency. a. Time-stepping

No analytic solution to test \rightarrow test code has designed accuracy $O(\Delta t, \Delta x^2)$.

Forward differencing $\rightarrow O(\Delta t)$ errors.

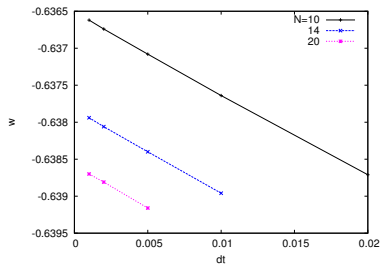
Look at $\omega(x = 0.5, y = 0.5, t = 1)$ – **exactly** (0.5, 0.5, 1)
1st order BC for ω_0 with $Re = 10$ and $N = 10, 14$ and 20.



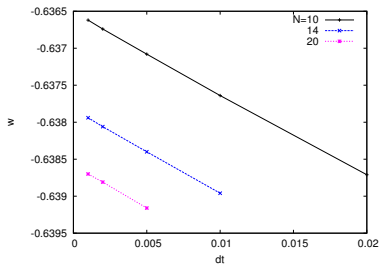
Note: linear in Δt , very very small Δt (larger unstable),
Large errors in $\Delta x \rightarrow$ 2nd order BC for ω_0 better?

2nd order BC for ω_0 with $Re = 10$ and $N = 10, 14$ and 20 .

2nd order BC for ω_0 with $Re = 10$ and $N = 10, 14$ and 20 .



2nd order BC for ω_0 with $Re = 10$ and $N = 10, 14$ and 20 .



Much smaller errors from Δx .

Well matched design

Errors for this problem are 2nd order in Δx and 1st order in Δt ,

Well matched design

Errors for this problem are 2nd order in Δx and 1st order in Δt ,
but stability has $\Delta t = \frac{1}{5} Re \Delta x^2$.

Well matched design

Errors for this problem are 2nd order in Δx and 1st order in Δt ,
but stability has $\Delta t = \frac{1}{5} Re \Delta x^2$.

Hence time errors $O(\Delta t) \approx$ space errors $O(\Delta x^2)$

Well matched design

Errors for this problem are 2nd order in Δx and 1st order in Δt ,
but stability has $\Delta t = \frac{1}{5} Re \Delta x^2$.

Hence time errors $O(\Delta t) \approx$ space errors $O(\Delta x^2)$

Hence no need for second-order time-stepping.

Accuracy consistence. b. Overall $O(\Delta x^2)$

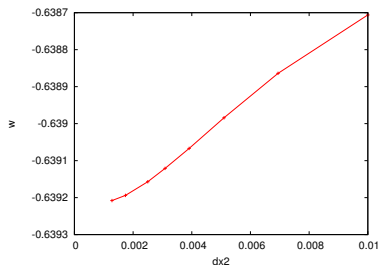
Set $\Delta t = 0.2Re\Delta x^2$.

Accuracy consistence. b. Overall $O(\Delta x^2)$

Set $\Delta t = 0.2Re\Delta x^2$. Plot $\omega(0.5, 0.5, 1)$ at $Re = 10$ for $N = 10, 12, 14, 16, 18, 20, 24$ and 28 .

Accuracy consistence. b. Overall $O(\Delta x^2)$

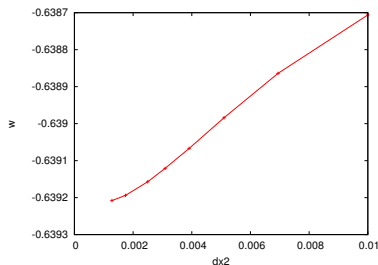
Set $\Delta t = 0.2Re\Delta x^2$. Plot $\omega(0.5, 0.5, 1)$ at $Re = 10$ for $N = 10, 12, 14, 16, 18, 20, 24$ and 28.



Linear in Δx^2 . Result: $\omega(0.5, 0.5, 1) = -0.63925 \pm 0.00005$.

Accuracy consistence. b. Overall $O(\Delta x^2)$

Set $\Delta t = 0.2Re\Delta x^2$. Plot $\omega(0.5, 0.5, 1)$ at $Re = 10$ for $N = 10, 12, 14, 16, 18, 20, 24$ and 28.

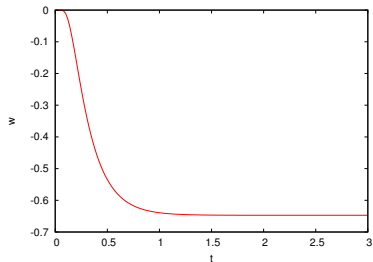


Linear in Δx^2 . Result: $\omega(0.5, 0.5, 1) = -0.63925 \pm 0.00005$.

Note linear extrapolation in Δx^2 from $N = 10$ and 14 gives same accuracy as 28 at $\frac{1}{32}$ the CPU.

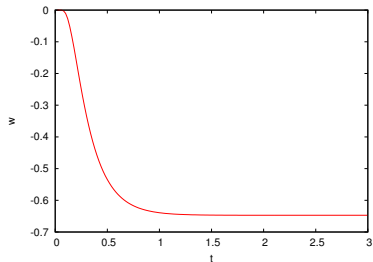
2.10 Results: time to evolve

Vorticity at centre of box as a function of time, with $N = 20$ and $Re = 10$.



2.10 Results: time to evolve

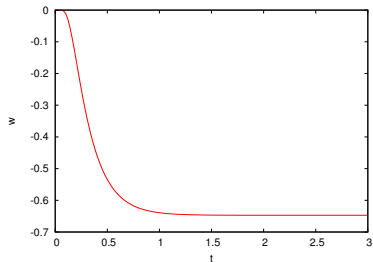
Vorticity at centre of box as a function of time, with $N = 20$ and $Re = 10$.



Steady to 10^{-4} by $t = 2$, time to diffuse across box.

2.10 Results: time to evolve

Vorticity at centre of box as a function of time, with $N = 20$ and $Re = 10$.

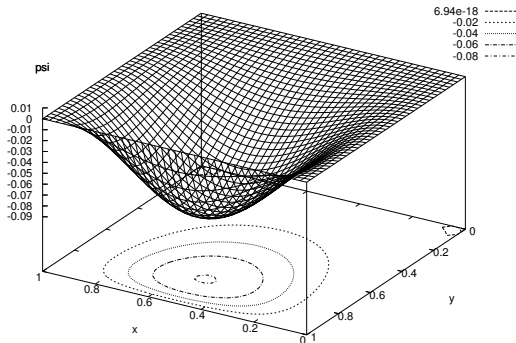


Steady to 10^{-4} by $t = 2$, time to diffuse across box.

For steady state, try reducing to 3 SOR per time step in place of N .

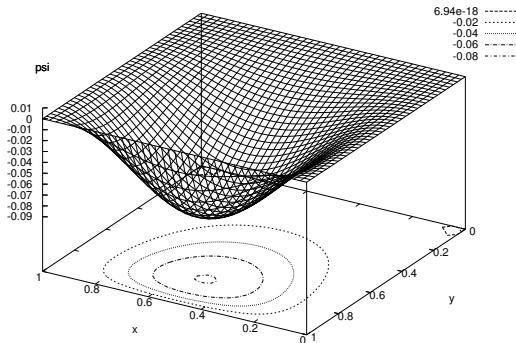
Results: steady streamfunction

At $t = 3$, $Re = 10$ and $N = 40$.



Results: steady streamfunction

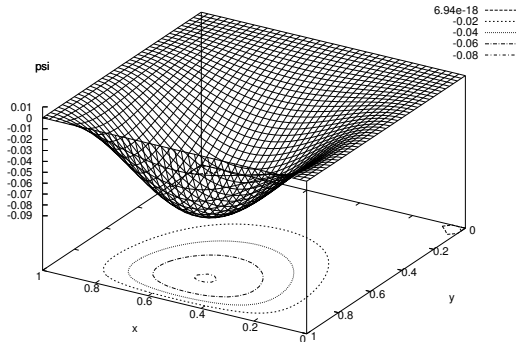
At $t = 3$, $Re = 10$ and $N = 40$.



Fast near lid, slow deep into cavity.

Results: steady streamfunction

At $t = 3$, $Re = 10$ and $N = 40$.

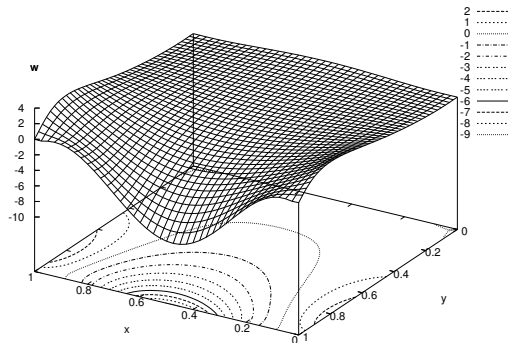


Fast near lid, slow deep into cavity.

Weak reversed circulations in bottom corners

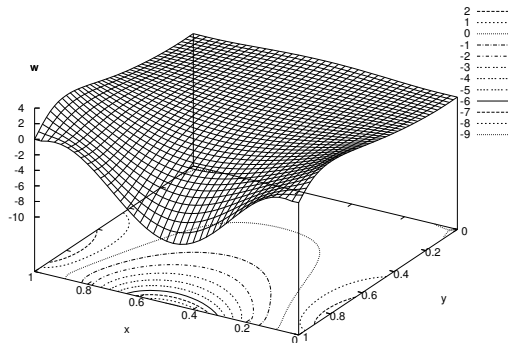
Results: steady vorticity

At $t = 3$, $Re = 10$ and $N = 40$.



Results: steady vorticity

At $t = 3$, $Re = 10$ and $N = 40$.



Slight asymmetry downstream

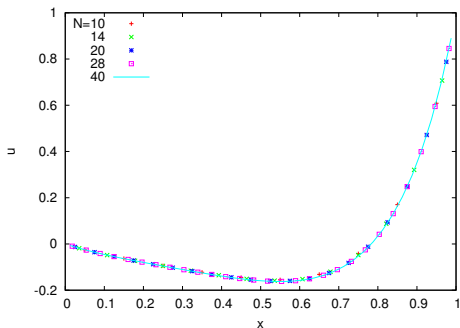
Results: steady mid-section velocity $u(0.5, y)$

$$u_{ij+\frac{1}{2}} = \frac{\psi_{ij+1} - \psi_{ij}}{\Delta x} \quad \text{for } y = (j + \frac{1}{2})\Delta x$$

Results: steady mid-section velocity $u(0.5, y)$

$$u_{ij+\frac{1}{2}} = \frac{\psi_{ij+1} - \psi_{ij}}{\Delta x} \quad \text{for } y = (j + \frac{1}{2})\Delta x$$

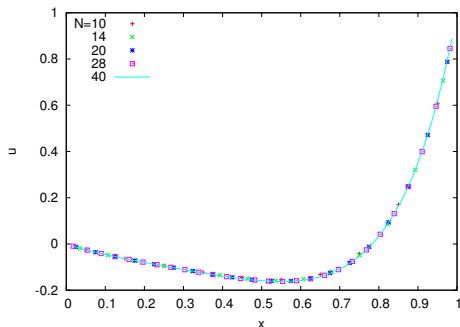
At $Re = 10$, with $N = 10, 14, 20, 28, 40$.



Results: steady mid-section velocity $u(0.5, y)$

$$u_{ij+\frac{1}{2}} = \frac{\psi_{ij+1} - \psi_{ij}}{\Delta x} \quad \text{for } y = (j + \frac{1}{2})\Delta x$$

At $Re = 10$, with $N = 10, 14, 20, 28, 40$.



Agree to visual accuracy

Force on lid

$$F = \int_0^1 \left. \frac{\partial u}{\partial y} \right|_{y=1} dx \approx \sum_{i=0}^N \left. \frac{\partial^2 \psi}{\partial y^2} \right|_{j=N} \Delta x.$$

Force on lid

$$F = \int_0^1 \frac{\partial u}{\partial y} \Big|_{y=1} dx \approx \sum_{i=0}^N \frac{\partial^2 \psi}{\partial y^2} \Big|_{j=N} \Delta x.$$

With $O(\Delta x)$ error

$$\frac{\partial^2 \psi}{\partial y^2} \Big|_{j=N} \approx \frac{\partial^2 \psi}{\partial y^2} \Big|_{j=N-1} = \frac{\psi_{iN} - 2\psi_{iN-1} + \psi_{i,N-2}}{\Delta x^2} + O(\Delta x).$$

Force on lid

$$F = \int_0^1 \frac{\partial u}{\partial y} \Big|_{y=1} dx \approx \sum_{i=0}^N \frac{\partial^2 \psi}{\partial y^2} \Big|_{j=N} \Delta x.$$

With $O(\Delta x)$ error

$$\frac{\partial^2 \psi}{\partial y^2} \Big|_{j=N} \approx \frac{\partial^2 \psi}{\partial y^2} \Big|_{j=N-1} = \frac{\psi_{iN} - 2\psi_{iN-1} + \psi_{i,N-2}}{\Delta x^2} + O(\Delta x).$$

For $O(\Delta x^2)$, linearly extrapolate to boundary

$$\begin{aligned} \frac{\partial^2 \psi}{\partial y^2} \Big|_{j=N} &\approx 2 \frac{\partial^2 \psi}{\partial y^2} \Big|_{j=N-1} - \frac{\partial^2 \psi}{\partial y^2} \Big|_{j=N-2} \\ &= \frac{2\psi_{iN} - 5\psi_{iN-1} + 4\psi_{i,N-2} - \psi_{i,N-3}}{\Delta x^2} + O(\Delta x^2). \end{aligned}$$

Force on lid

$$F = \int_0^1 \frac{\partial u}{\partial y} \Big|_{y=1} dx \approx \sum_{i=0}^N \frac{\partial^2 \psi}{\partial y^2} \Big|_{j=N} \Delta x.$$

With $O(\Delta x)$ error

$$\frac{\partial^2 \psi}{\partial y^2} \Big|_{j=N} \approx \frac{\partial^2 \psi}{\partial y^2} \Big|_{j=N-1} = \frac{\psi_{iN} - 2\psi_{iN-1} + \psi_{i,N-2}}{\Delta x^2} + O(\Delta x).$$

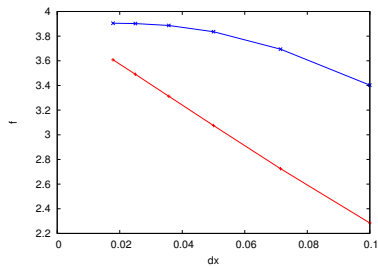
For $O(\Delta x^2)$, linearly extrapolate to boundary

$$\begin{aligned} \frac{\partial^2 \psi}{\partial y^2} \Big|_{j=N} &\approx 2 \frac{\partial^2 \psi}{\partial y^2} \Big|_{j=N-1} - \frac{\partial^2 \psi}{\partial y^2} \Big|_{j=N-2} \\ &= \frac{2\psi_{iN} - 5\psi_{iN-1} + 4\psi_{i,N-2} - \psi_{i,N-3}}{\Delta x^2} + O(\Delta x^2). \end{aligned}$$

Check: $\psi = 1, y, y^2, y^3 \rightarrow 0, 0, 2, 0$

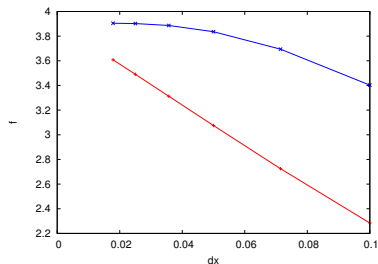
Results: force on lid

At $Re = 10$ for $N = 10, 14, 20, 28, 40$ and 56 .



Results: force on lid

At $Re = 10$ for $N = 10, 14, 20, 28, 40$ and 56 .



The final answer for the force is

$$F = 3.905 \pm 0.002 \quad \text{at } Re = 10.$$

Results: early times

Results: early times

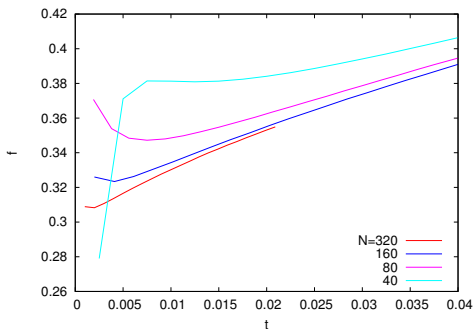
Simple $\sqrt{\nu t}$ solution.

Results: early times

Simple $\sqrt{\nu t}$ solution. Plot $F/\sqrt{t/Re}$

Results: early times

Simple $\sqrt{\nu t}$ solution. Plot $F/\sqrt{t/Re}$

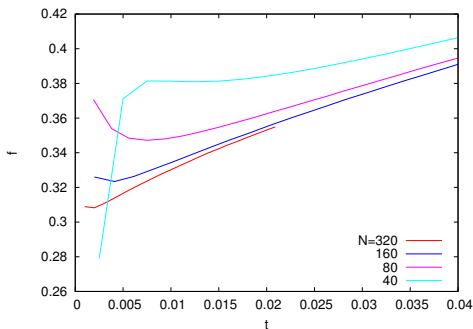


for $N = 40, 80, 160$ and 320 .

Failure: Code not designed for \sqrt{t} behaviour.

Results: early times

Simple $\sqrt{\nu t}$ solution. Plot $F/\sqrt{t/Re}$

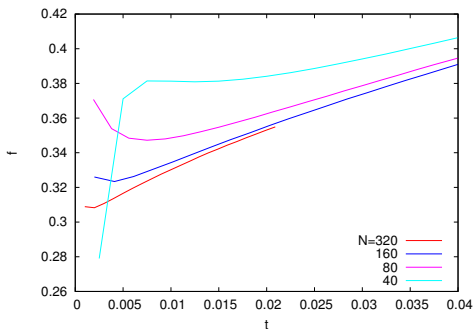


for $N = 40, 80, 160$ and 320 .

Failure: Code not designed for \sqrt{t} behaviour.

Results: early times

Simple $\sqrt{\nu t}$ solution. Plot $F/\sqrt{t/Re}$



for $N = 40, 80, 160$ and 320 .

Failure: Code not designed for \sqrt{t} behaviour.

Note **0.33**, **0.319**, **0.307** $\rightarrow \frac{1}{2\sqrt{\pi}} = 0.281$ with $0.4\Delta x^{1/2}$ error.