Conservation equations - true all materials

Conservation of momentum (Cauchy):

$$\rho \frac{D\mathbf{u}}{Dt} = \nabla \cdot \boldsymbol{\sigma} + \rho \mathbf{g}$$

- ▶ Often inertia (LHS) is negligible.
- Usually incompressible (plus conservation of mass):

 $abla \cdot \mathbf{u} = \mathbf{0}$ 

so add pressure to stress, often omitted below.

• Need Constitutive (material dependent) Relation between stress  $\sigma$  and flow **u**.

### 'Simple' materials

Lagrangian description

 $\mathbf{X} 
ightarrow \mathbf{x}(\mathbf{X},t)$ 

Deformation of line element (for micro-lengths  $\ll$  macro-lengths)

$$\delta \mathbf{X} \to \delta \mathbf{x} = A \cdot \delta \mathbf{X}, \qquad A_{iJ} = \frac{\partial x_i}{\partial X_J}$$

A has rotation and stretch, see later. Local and casual dependency

$$\sigma(t) = \sigma \{A(\tau)\}_{\tau \le t}$$

This functional dependence not useful, except for fast elastic limit and slow viscous limits (each with single parameter)

## Chapter 3

#### Constitutive equations

Phenomenology 'Simple' materials Perfectly elastic material Time derivatives Exact approximations Linear viscoelasticity Second-order fluid Semi-empirical models Generalised Newtonian Oldroyd-B

# Material Frame Indifference

K-BKZ

'Tensorial correct' or result independent of observer, so same stresses if add translation and rotation

$$\mathbf{x}' = \mathbf{a}(t) + Q(t)\mathbf{x}$$

so in new frame

$$\sigma' = \sigma \left\{ Q(\tau) A(\tau) Q^{\mathsf{T}}(0) \right\}_{\tau \leq t} \equiv Q(t) \sigma \left\{ A(\tau) \right\}_{\tau \leq t} Q^{\mathsf{T}}(t).$$

Require  $\sigma \{A\}$  to obey this identity for all Q(t).

## Perfectly elastic material

Instantaneous, no history.

Decompose deformation A into first a stretch U followed by a rotation R,

$$A = RU$$
, with  $R^T R = I$ , by finding  $A$ :  $U^2 = A^T A$ 

The set  $Q = R^T$  in Material Frame Indifference

$$\sigma\left\{A\right\} = R(t)f(U(t))R^{7}$$

In incompressible material with isotropic in rest state,

$$f(U^2) = U^2 f_1 + U^{-2} f_2$$
,  $f_i$  scalar functions of invariants of  $U$ ,

SO

$$\sigma = AA^T f_1 + A^{-1} A^{-1} f_2$$

## Perfectly elastic material 2

Alternatively for incompressible with isotropic in rest state, use an elastic potential energy w, a function of eigenvalues  $\lambda_i$  of U in invariant combinations

 $\alpha = \frac{1}{2} \left( \lambda_1^2 + \lambda_2^2 + \lambda_3^2 \right), \beta = \frac{1}{2} \left( \lambda_1^{-2} + \lambda_2^{-2} + \lambda_3^{-2} \right), \gamma = \lambda_1 \lambda_2 \lambda_3 \equiv 1$ 

Virtual work and  $\sigma$  co-diagonal with U gives

$$\sigma_1 = \frac{1}{\lambda_2 \lambda_3} \left( \frac{\partial w}{\partial \lambda_1} = \lambda_1 \frac{\partial w}{\partial \alpha} - \lambda_1^{-3} \frac{\partial w}{\partial \beta} \right),$$

so

$$\sigma = \frac{1}{\gamma} \frac{\partial \mathbf{w}}{\partial \alpha} A A^{\mathsf{T}} - \frac{1}{\gamma} \frac{\partial \mathbf{w}}{\partial \beta} A^{-1 \mathsf{T}} A^{-1}.$$

Better for data fitting – Ogden model:  $w(\lambda_1^n + \lambda_2^n + \lambda_3^n)$ 

## Time derivatives

To express history dependence will use time derivatives and integrals.

But problem : In new frame

$$\sigma' = Q \sigma Q^T$$

so its time derivative

$$\dot{\sigma}' = Q\dot{\sigma}Q^{\mathsf{T}} + \dot{Q}\sigma Q^{\mathsf{T}} + Q\sigma\dot{Q}^{\mathsf{T}}$$

is different in different frames.

Now flow transforms

 $u' = Qu + \dot{Q}x + \dot{a}$ 

so velocity gradients transform

$$\frac{\partial u'}{\partial x'} = Q \frac{\partial u}{\partial x} Q^T + \dot{Q} Q^T \qquad \left( \text{watch indices, } \equiv \nabla u^T \right)$$

SO

strain-rate 
$$E' = QEQ^T$$
, vorticity (tensor)  $\Omega' = Q\Omega Q^T - \dot{Q}Q^T$ 

# Co-rotational (Jaumann) time derivative

Hence co-rotational (Jaumann) time derivative

$$\overset{\circ}{\sigma} \equiv \frac{D\sigma}{Dt} - \Omega^T \cdot \sigma - \sigma \cdot \Omega$$

has transformation

$$\overset{\circ'}{\sigma'} = Q \overset{\circ}{\sigma} Q^T$$
 Student Exercise

This is the rate of change of  $\sigma$  seen by an observer rotating with the vorticity, and so is universal.

Recall rotation frames

$$\ddot{\mathbf{x}} = \dot{\mathbf{x}} + \Omega \mathbf{x}$$

# Co-deformational time derivative

Can add multiple of  $E\sigma + \sigma E$  to co-rotational derivative. Hence (upper) co-deformational (Oldroyd-B) derivative

$$\stackrel{\nabla}{\sigma} \equiv \frac{D\sigma}{Dt} - \nabla u^T \cdot \sigma - \sigma \cdot \nabla u$$

has transformation

$$\stackrel{
abla'}{\sigma'} = Q \stackrel{
abla}{\sigma} Q^T$$

Student Exercise

Recall stretching material line element

$$\dot{\delta\ell} = \delta\ell \cdot \nabla\iota$$

so for second-order tensor

$$\delta\dot{\ell}\delta\ell = \nabla u^{\mathsf{T}} \cdot \delta\ell\delta\ell + \delta\ell\delta\ell \cdot \nabla u$$

Linear viscoelasticity 2



$$G(t) = G_0 e^{-t/\tau}$$

show that a polar plot of  $Re(G^*)$  versus  $Im(G^*)$  as (real)  $\omega$  varies is part of a circle.

### Linear viscoelasticity

The most general linear response for all materials isotropic in rest state.

Linearise in low stretch:  $A^T A \approx I$ 

$$\sigma(t) = R(t) \int_0^\infty \frac{G(s)\overline{A^T A}(t-s) \, ds \, R^T(t)$$

The  $R(t) \dots R^{T}(t)$  is a co-rotational integral, but usually dropped in linearisation.

Memory kernel G(s) is the Fourier transform of  $G^*(\omega)$  of oscillating shear flow.

For a Newtonian viscous fluid  $G(s) = \delta(s)$  and for an elastic solid G(s) = 1.

### Linear viscoelasticity 3

Scalar form for simple shear flow

$$\sigma(t) = \int_0^\infty G(s) \dot{\gamma}(t-s) \, ds$$

Hence steady shear viscosity (plug in  $\dot{\gamma} = \text{const}$ )

$$\mu(0)=\int_0^\infty G(s)\,ds$$

Hence recoil after stop steady shear flow  $\dot{\gamma}_0$ 

 $-\dot{\gamma}_0 \frac{\int_0^\infty sG(s)\,ds}{\int_0^\infty G(s)\,ds}$ 

Student Exercise

# Second-order fluid

For weak and slowly varying flows, the first nonlinear correction

$$\sigma = -p\mathbf{I} + 2\mu \mathbf{E} - 2\alpha \overset{\nabla}{\mathbf{E}} + \beta \mathbf{E} \cdot \mathbf{E}$$

where

$$\mu = \int_0^\infty G(s) \, ds, \quad \alpha = \int_0^\infty s G(s) \, ds$$

from 'retarded motion' expansion.

Hence Cox-Mertz is correct in the limit  $\dot{\gamma} \rightarrow 0$ ,  $\omega \rightarrow 0$ .

Good for dithering Stokes flow, where accumulation of small effects over a long time can produce a significant change.

Dangerous in stability analyses and numerical studies, where bad behaviour can occur outside limitation of weak and slowly varying.

# Generalised Newtonian

Newtonian viscous fluid, except viscosity depends on shear-rate  $\dot{\gamma}$ ,

$$\sigma = -pI + 2\mu(\dot{\gamma})E$$
 where  $\dot{\gamma} = \sqrt{2E:E}$ .

Depends on instantaneous flow, i.e. no elastic part and no history. 'Ad hoc' models to fit experimental data

► Power-law

$$\mu = k \dot{\gamma}^{n-1}$$
, i.e. stress  $\sigma \propto \dot{\gamma}^n$ 

► Carreau, Yasuda & Cross

$$\mu = \mu_{\infty} + (\mu_0 - \mu_{\infty}) \left(1 + (\tau \dot{\gamma})^a\right)^{(n-1)/a}$$

with plateaus at high and low  $\dot{\gamma}.$ 

#### Student Exercises

In simple shear

- $\blacktriangleright$  constant viscosity  $\mu$
- ▶ Normal stress difference  $N_1 = 2\alpha\dot{\gamma}^2$ ,  $N_2 = -\frac{1}{4}\beta\dot{\gamma}^2$

### In (axisymmetric pure) extensional flow

- $\blacktriangleright \ \mu_{\text{ext}} = \mu + \left(\alpha + \frac{1}{4}\beta\right)\dot{\epsilon}$
- but must keep last term small

# Generalised Newtonian

More 'ad hoc' models.

Yield fluids which only flow if  $\sigma$  exceeds a yield value  $\sigma_Y$ .

Bingham

$$\sigma = \begin{cases} \infty, \text{ so } E = 0 & \text{if } \sigma < \sigma_Y \\ \mu_0 + \sigma_Y / \dot{\gamma} & \text{if } \sigma > \sigma_Y \end{cases}$$

Herchel-Buckley

$$\sigma = \begin{cases} \infty, \text{ so } E = 0 & \text{ if } \sigma < \sigma_Y \\ \mu_0 \dot{\gamma}^{n-1} + \sigma_Y / \dot{\gamma} & \text{ if } \sigma > \sigma_Y \end{cases}$$

# Oldroyd-B model fluid

History dependence through time differentials. Easier for computing than with time integrals

$$\sigma + \lambda_1 \overset{\nabla}{\sigma} = 2\mu_0 \left( E + \lambda_2 \overset{\nabla}{E} \right) \quad \text{with } 0 \le \lambda_2 \le \lambda_1$$

Three constants

- a viscosity  $\mu_0$ ,
- $\blacktriangleright$  a relaxation time  $\lambda_1$  and
- a retardation time  $\lambda_2$ .

### Special cases

- Maxwell UCM  $\lambda_2 = 0$
- Newtonian  $\lambda_1 = \lambda_2$

# Oldroyd-B model fluid 2

### Student Exercises

In simple shear

- constant viscosity  $\mu = \mu_0$
- Normal stress difference  $N_1 = 2\mu_0(\lambda_1 \lambda_2)\dot{\gamma}^2$ ,  $N_2 = 0$

In (axisymmetric pure) extensional flow

$$\mu_{ ext{ext}} = \mu_0 rac{1 - \lambda_2 \dot{\epsilon} - 2\lambda_1 \lambda_2 \dot{\epsilon}^2}{(1 - 2\lambda_1 \dot{\epsilon})(1 + \lambda_1 \epsilon)}$$

• becomes negative just above  $\dot{\epsilon} = 1/2\lambda_1 !!!!!!$ 

# Variants of Oldroyd-B

• White-Metzner to incorporate shear-thinning  $\mu(\dot{\gamma})$ 

$$\sigma + \frac{\mu(\dot{\gamma})}{G} \overset{\nabla}{\sigma} = 2\mu(\dot{\gamma})E$$

Giesekus for positive extensional viscosity

$$\sigma + \frac{\alpha \lambda_1}{\mu_0} \sigma^2 + \lambda_1 \overset{\nabla}{\sigma} = 2\mu_0 E$$

PTT-exponential Phan-Thien & Tanner

$$\sigma + \left[\exp\left(\frac{\lambda_1}{\mu_0} \operatorname{trace} \sigma\right) - 1\right] \sigma + \lambda_1 \overset{\nabla}{\sigma} = 2\mu_0 E$$

Multi-mode versions of above

Microstructure A:

$$\stackrel{\nabla}{A} + \frac{f}{\tau}(A - I) = 0$$

Stress  $\sigma$ :

$$\sigma = -pI + 2\mu_0 E + Gf(A - I)$$

Oldroyd-B f = 1

FENE modification, for nice behaviour in extensional flow

$$f = \frac{L^2}{L^2 - \text{trace } A}$$

### K-BKZ model fluid Kay-Bernstein-Kearsley-Zappa

History dependence through time integrals Merging of linear viscoelasticity and nonlinear elasticity

$$\sigma = \int_0^\infty \dot{G}(s) \left[ \frac{\partial w}{\partial \alpha} \left( \tilde{A} \tilde{A}^T - I \right) - \frac{\partial w}{\partial \beta} \left( \tilde{A}^{-1 T} \tilde{A}^{-1} - I \right) \right] ds$$

where the relative deformation from s to t is

$$\tilde{A} = A(t)A^{-1}(t-s)$$

 $\frac{\partial w}{\partial \alpha}$  and  $\frac{\partial w}{\partial \beta}$  are usually replaced by  $\phi_1$  and  $\phi_2$  'damping functions, not derivatives of some w,

functions of combinations  $\alpha$  and  $\beta$  eigenvalues of  $\tilde{A}$ .

# K-BKZ model fluid 2

### Student Exercises

In simple shear

$$\mu = \int_0^\infty \dot{G}(s) (\phi_1 + \phi_2) s \, ds$$
$$N_1 = \int_0^\infty \dot{G}(s) (\phi_1 + \phi_2) s^2 \, ds, \qquad N_2 = -\int_0^\infty \dot{G}(s) \phi_2 s^2 \, ds,$$

In extensional flow

$$\mu_{\text{ext}} = \int_0^\infty \dot{G}(s) \left[ \phi_1 \left( e^{2\dot{\epsilon}s} - e^{-\dot{\epsilon}s} \right) + \phi_2 \left( e^{\dot{\epsilon}s} - e^{-2\dot{\epsilon}s} \right) \right] s \, ds/\dot{\epsilon}$$

# K-BKZ model fluid 3

Wagner model

$$\phi_2 = 0$$
 so  $N_2 = 0$ 

and

$$\phi_1 = \exp\left(-k\sqrt{\alpha - 3 + \theta(\beta - \alpha)}\right)$$

In shear shear

$$\phi_1 = \exp\left(-k\dot{\gamma}(t-s)\right)$$