

Microstructural studies for rheology

- ▶ Micro & macro views
- ▶ Einstein viscosity
- ▶ Rotations
- ▶ Deformations
- ▶ Interactions
- ▶ Polymers
- ▶ Others

Rotations

- ▶ Rotation of particles
- ▶ Macro stress
- ▶ Uni-axial straining
 - ▶ Extensional viscosity rods
 - ▶ Extensional viscosity disks
- ▶ Simple shear
 - ▶ Shear viscosity
- ▶ Anisotropy
- ▶ Brownian rotations
 - ▶ Macro stress
 - ▶ Viscosities
 - ▶ Closures

Rotation of particles – rigid and dilute

Spheroid: axes a, b, b , aspect ratio $r = \frac{a}{b}$.



rod $r > 1$



disk $r < 1$

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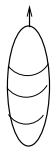


disk $r < 1$

Direction of axis $\mathbf{p}(t)$, unit vector.

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Stokes flow by Oberbeck (1876). See Lamb. Uses ellipsoidal harmonic function in place of spherical harmonic $1/r$

$$\int_{s(\mathbf{x})}^{\infty} \frac{ds'}{\prod_{i=1}^3 (a_i^2 + s')^{1/2}}, \quad \text{where} \quad \sum_{i=1}^3 \frac{x_i^2}{a_i^2 + s(\mathbf{x})} = 1.$$

Rotation of particles

Microstructural evolution equation

$$\frac{D\mathbf{p}}{Dt} = \boldsymbol{\Omega} \times \mathbf{p} + \frac{r^2-1}{r^2+1} [\mathbf{E} \cdot \mathbf{p} - \mathbf{p}(\mathbf{p} \cdot \mathbf{E} \cdot \mathbf{p})]$$

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Long rods $\frac{r^2-1}{r^2+1} \rightarrow +1$ i.e. **Upper Convective Derivative** $\nabla_{\mathbf{A}}$

Flat disks $\frac{r^2-1}{r^2+1} \rightarrow -1$ i.e. **Lower Convective Derivative** $\triangle_{\mathbf{A}}$

Rotation of particles

Student Exercise

Show that

$$\mathbf{p}(t) = \frac{\mathbf{q}(t)}{|\mathbf{q}(t)|} \quad \text{with} \quad \dot{\mathbf{q}} = \boldsymbol{\Omega} \times \mathbf{q} + \frac{r^2-1}{r^2+1} \mathbf{E} \cdot \mathbf{q}$$

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Hence find $\mathbf{p}(t)$ for axisymmetric extensional flow and for simple shear, starting from an arbitrary initial $\mathbf{p}(0)$.

Micro→macro link: stress

$$\bar{\sigma} = -\bar{p}I + 2\mu\mathbf{E} + 2\mu\phi [A(\mathbf{p} \cdot \mathbf{E} \cdot \mathbf{p})\mathbf{p}\mathbf{p} + B(\mathbf{p}\mathbf{p} \cdot \mathbf{E} + \mathbf{E} \cdot \mathbf{p}\mathbf{p}) + C\mathbf{E}]$$

with A, B, C material constants depending on shape but not size

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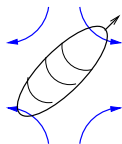
	A	B	C
$r \rightarrow \infty$	$\frac{r^2}{2(\ln 2r - \frac{3}{2})}$	$\frac{6 \ln 2r - 11}{r^2}$	2
$r \rightarrow 0$	$\frac{10}{3\pi r}$	$-\frac{8}{3\pi r}$	$\frac{8}{3\pi r}$

Rotation in uni-axial straining

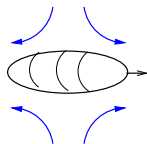
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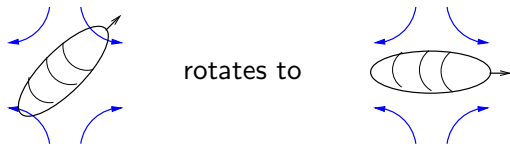


rotates to



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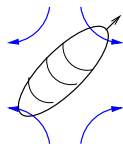
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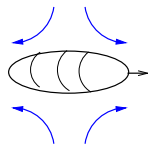
Aligns with stretching direction → **maximum dissipation**

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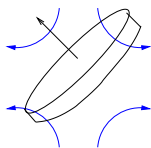
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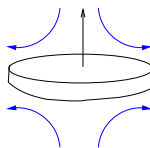
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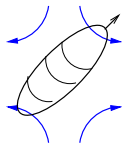


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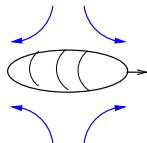


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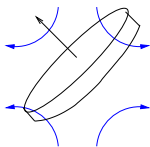
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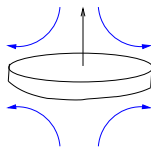
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Effective extensional viscosity for rods

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Dilute requires $na^3 \ll 1$, but extension by Batchelor to semi-dilute $\phi \ll 1 \ll \phi r^2$

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$$\mu_{\text{ext}}^* = \mu \left(1 + \phi \frac{10}{3\pi r} \right) = \mu \left(1 + \frac{10nb^3}{9} \right)$$

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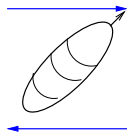
No semi-dilute theory, yet.

Behaviour in simple shear

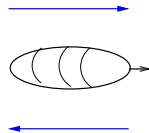
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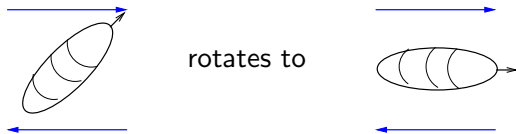


rotates to



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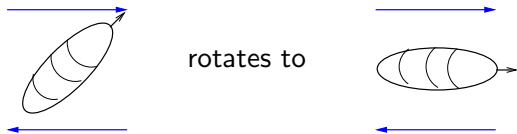
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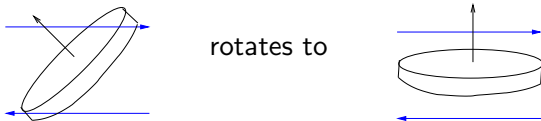
Rotates to flow direction → **minimum dissipation**

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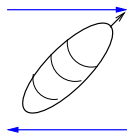


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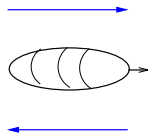


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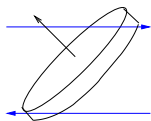
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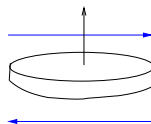
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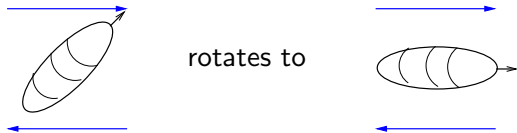
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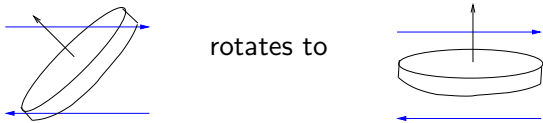
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Rotates to flow direction \rightarrow **minimum dissipation**



Rotates to lie in flow \rightarrow **minimum dissipation**

Both Tumble: flip in $1/\gamma$, then align for r/γ ($\delta\theta = 1/r$ with $\dot{\theta} = \gamma/r^2$)

Effective shear viscosity

Jeffery orbits (1922)

$$\begin{aligned}\dot{\phi} &= \frac{\gamma}{r^2+1} (r^2 \cos^2 \phi + \sin^2 \phi) \\ \dot{\theta} &= \frac{\gamma(r^2-1)}{4(r^2+1)} \sin 2\theta \sin 2\phi\end{aligned}$$

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Solution with orbit constant C .

$$\tan \phi = r \tan \omega t, \quad \omega = \frac{\gamma r}{r^2+1}, \quad \tan \theta = Cr(r^2 \cos^2 \phi + \sin^2 \phi)^{-1/2}$$

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Effective shear viscosity Leal & H (1971)

$$\mu_{\text{shear}}^* = \mu \left(1 + \phi \begin{cases} 0.32r / \ln r & \text{rods} \\ 3.1 & \text{disks} \end{cases} \right)$$

numerical coefficients depend on distribution across orbits, C .

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This material anisotropy leads to **anisotropy of macro flow**.

Important to Turbulent Drag Reduction

Three measures of concentration of rods

$$\begin{cases} \phi r^2 \doteq na^3 & \text{for } \mu_{\text{ext}}^* \\ \phi r \doteq na^2 b & \text{for } \mu_{\text{shear}}^* \\ \phi \doteq nab^2 & \text{for permeability} \end{cases}$$

Brownian rotations – for stress relaxation

Rotary diffusivity: for spheres,

$$D_{\text{rot}} = kT / 8\pi\mu a^3,$$

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$$D_{\text{rot}} = kT / 8\pi\mu a^3, \quad kT / \frac{8\pi\mu a^2}{3(\ln 2r - 1.5)},$$

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Fokker-Plank equation

$$\frac{\partial P}{\partial t} + \nabla \cdot (\dot{\mathbf{p}}P) = D_{\text{rot}} \nabla^2 P$$

$\dot{\mathbf{p}}(\mathbf{p})$ earlier deterministic.

Average stress over distribution P

Averaged stress

$$\begin{aligned}\sigma = & -pI + 2\mu E + 2\mu\phi[A E : \langle \mathbf{p}\mathbf{p}\mathbf{p}\mathbf{p} \rangle \\ & + B(E \cdot \langle \mathbf{p}\mathbf{p} \rangle + \langle \mathbf{p}\mathbf{p} \rangle \cdot E) + C E + F D_{\text{rot}} \langle \mathbf{p}\mathbf{p} \rangle]\end{aligned}$$

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Last FD_{rot} term is entropic stress.

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Extra material constant $F = 3r^2/(\ln 2r - 0.5)$ for rods and $12/\pi r$ for disks.

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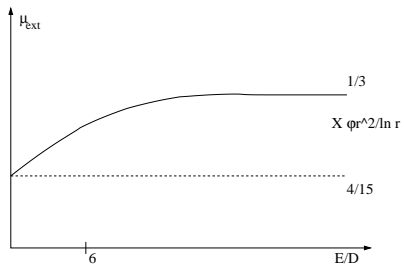
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Averaging

$$\langle \mathbf{pp} \rangle = \int_{|\mathbf{p}|=1} \mathbf{pp} P \, dp$$

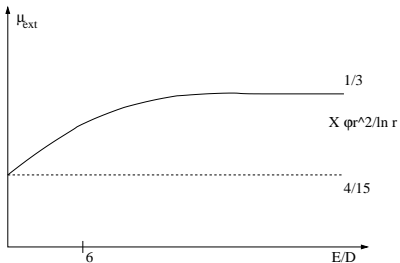
Solve Fokker-Plank: numerical, weak and strong Brownian rotations

Extensional and shear viscosities

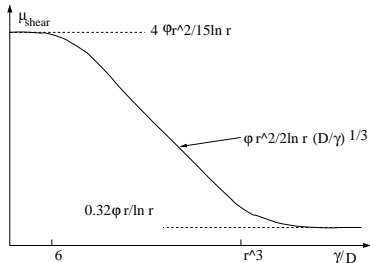


Small
strain-hardening

Extensional and shear viscosities

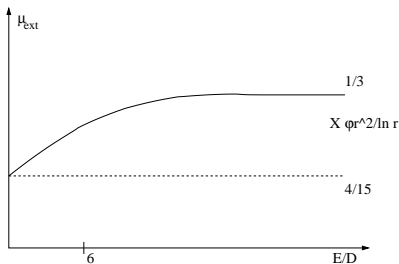


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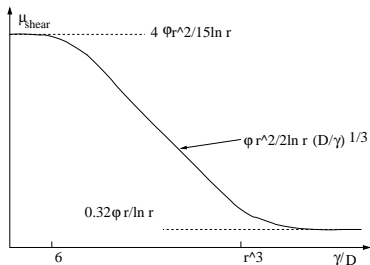


Large
shear-thinning

Extensional and shear viscosities



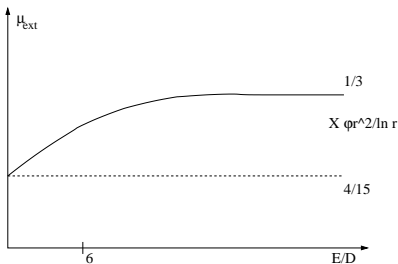
Small
strain-hardening



Large
shear-thinning

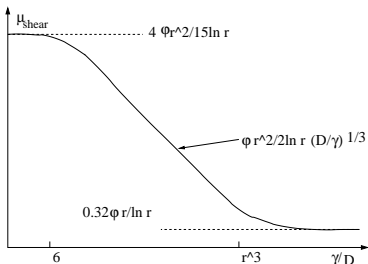
Also $N_1 > 0$,
 N_2 small < 0 .

Extensional and shear viscosities



Small
strain-hardening

↕ Orientation effects



Large
shear-thinning

Also $N_1 > 0$,
 N_2 small < 0 .

The closure problem

- ▶ Second moment of Fokker-Plank equation

$$\begin{aligned} & \frac{D}{Dt} \langle \mathbf{pp} \rangle - \Omega \cdot \langle \mathbf{pp} \rangle \langle \mathbf{pp} \rangle \cdot \Omega \\ &= \frac{r^2-1}{r^2+1} [E \cdot \langle \mathbf{pp} \rangle + \langle \mathbf{pp} \rangle \cdot E - 2 \langle \mathbf{pppp} \rangle : E] - 6D_{\text{rot}} \left[\langle \mathbf{pp} \rangle - \frac{1}{3} I \right] \end{aligned}$$

Hence this and stress need $\langle \mathbf{pppp} \rangle$, so an infinite hierarchy.

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- ▶ **Better**: correct in weak and strong limits

$$= \frac{1}{5} [6 \langle \mathbf{pp} \rangle \cdot E \cdot \langle \mathbf{pp} \rangle - \langle \mathbf{pp} \rangle \langle \mathbf{pp} \rangle : E - 2I(\langle \mathbf{pp} \rangle^2 : E - \langle \mathbf{pp} \rangle : E)]$$

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- ▶ **New idea Brownian fields**: simulate many random walks in orientation space for each point of the complex flow.

Rotations

- ▶ Rotation of particles
- ▶ Macro stress
- ▶ Uni-axial straining
 - ▶ Extensional viscosity rods
 - ▶ Extensional viscosity disks
- ▶ Simple shear
 - ▶ Shear viscosity
- ▶ Anisotropy
- ▶ Brownian rotations
 - ▶ Macro stress
 - ▶ Viscosities
 - ▶ Closures

Microstructural studies for rheology

- ▶ Micro & macro views
- ▶ Einstein viscosity
- ▶ Rotations
- ▶ Deformations
- ▶ Interactions
- ▶ Polymers
- ▶ Others

Deformations

- ▶ Emulsions
 - ▶ Rupture
 - ▶ Theories
 - ▶ Numerical
- ▶ Flexible thread
- ▶ Double layer

Emulsions - deformable microstructure

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[Reviews](#): Ann. Rev. Fluid Mech. Rallison (1984), Stone (1994)

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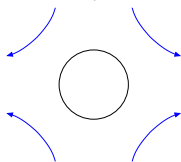
Rupture if $\mu_{\text{ext}} > \frac{T}{Ea}$ (normally)

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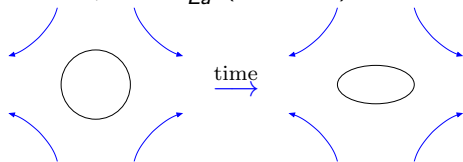


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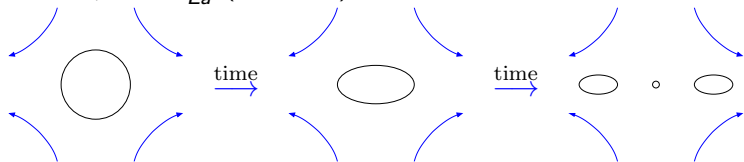


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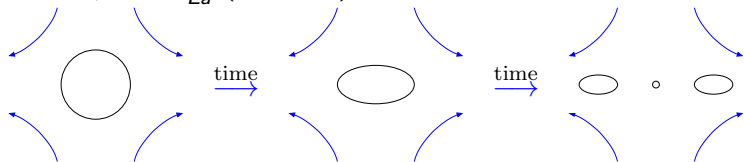


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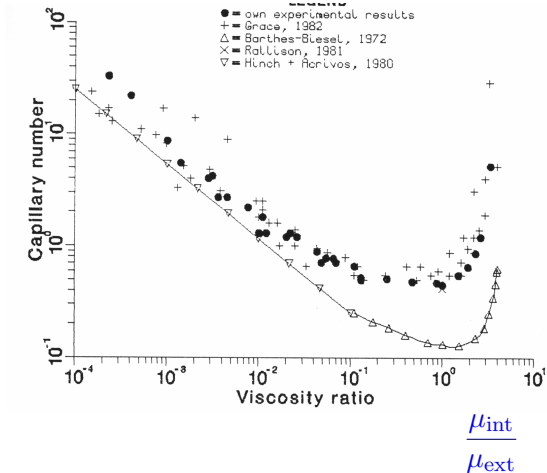
Rupture if $\mu_{\text{ext}} > \frac{T}{Ea}$ (normally)



Irreversible reduction in size to $a_* = T/\mu_{\text{ext}}E$, as coalescence very slow.

Rupture in shear flow

$$\frac{T}{\mu_{\text{ext}} Ea}$$



Experiments: de Bruijn (1989) (=own), Grace (1982)

Theories: Barthes-Biesel (1972), Rallison (1981), Hinch & Acrivos (1980)

Rupture difficult if $\mu_{\text{int}} \ll \mu_{\text{ext}}$

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$$\mu_{\text{ext}} E > \frac{T}{a} \left\{ 0.54 (\mu_{\text{ext}} / \mu_{\text{int}})^{2/3} \right. \quad \text{simple shear}$$

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but tip-streaming with mobile surfactants (makes rigid end-cap)

$$\mu_{\text{ext}} E > \frac{T}{a} 0.56$$

Rupture difficult is simple shear if $\mu_{\text{int}} > 3\mu_{\text{ext}}$

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- ▶ until can rupture when $\mu_{\text{int}} \leq 3\mu_{\text{ext}}$

Theoretical studies: small deformations

Small ellipsoidal deformation

$$r = a(1 + \mathbf{x} \cdot \mathbf{A}(t) \cdot \mathbf{x} + \text{higher orders})$$

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Stokes flow with help of computerised algebra manipulator

$$\begin{aligned} \frac{D\mathbf{A}}{Dt} - \boldsymbol{\Omega} \cdot \mathbf{A} + \mathbf{A} \cdot \boldsymbol{\Omega} = & 2k_1 \mathbf{E} + k_5(\mathbf{A} \cdot \mathbf{E} + \mathbf{E} \cdot \mathbf{A}) + \dots \\ & - \frac{T}{\mu_{\text{ext}} a} (k_2 \mathbf{A} + k_6(\mathbf{A} \cdot \mathbf{A}) + \dots) \end{aligned}$$

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$$\boldsymbol{\sigma} = -p\mathbf{I} + 2\mu_{\text{ext}} \mathbf{E} + 2\mu_{\text{ext}} \phi [k_3 \mathbf{E} + k_7(\mathbf{A} \cdot \mathbf{E} + \mathbf{E} \cdot \mathbf{A}) + \dots \\ - \frac{T}{\mu_{\text{ext}} a} (k_4 \mathbf{A} + k_8(\mathbf{A} \cdot \mathbf{A}) + \dots)]$$

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with k_n depending on viscosity ratio, $\lambda = \mu_{\text{int}}/\mu_{\text{ext}}$,

$$k_1 = \frac{5}{2(2\lambda+3)}, \quad k_2 = \frac{40(\lambda+1)}{(2\lambda+3)(19\lambda+16)} \\ k_3 = \frac{5(\lambda-1)}{3(2\lambda+3)}, \quad k_4 = \frac{4}{2\lambda+3}$$

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k_1 inefficiency of rotating by straining

Inefficiency of rotating by straining

Student Exercise

Consider the constitutive equation

$$\sigma = -pI + 2\mu_0 E + GA$$
$$\frac{DA}{Dt} - \Omega \cdot A + A \cdot \Omega - \alpha(E \cdot A + A \cdot E) = -\frac{1}{\tau}(A - I),$$

in flow $u = (\Omega + E) \cdot x$.

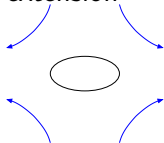
Solve for σ in steady simple shear, finding the shear viscosity and normal stress differences.

Find the condition on the parameters for the shear stress to be a monotonic increasing function of the shear-rate (non-shear-banding).

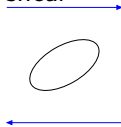
Theoretical studies: small deformations 2

Equilibrium shapes before rupture

extension



shear

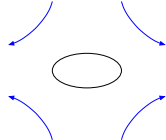


internal circulation,
tank-treading

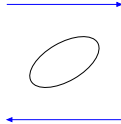
Theoretical studies: small deformations 2

Equilibrium shapes before rupture

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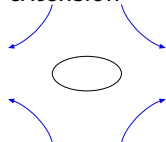
Rheology before rupture

Small strain-hardening, small shear-thinning, $N_1 > 0$, $N_2 < 0$.

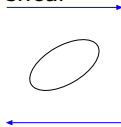
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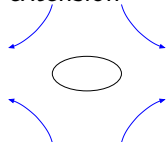
Repeated rupture leaves $\mu^* \cong \text{constant}$.

Einstein: independent of size of particle, just depends on ϕ .

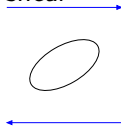
Theoretical studies: small deformations 2

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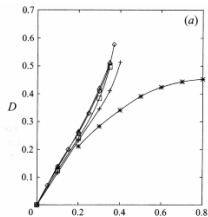
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Form of constitutive equation

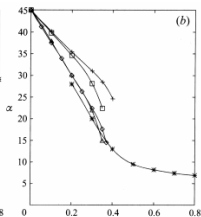
$$\frac{d}{dt}(\text{state}) \quad \& \quad \sigma \quad \text{linear in} \quad \mathbf{E} \quad \& \quad \frac{T}{\mu_{\text{ext}} a}$$

Numerical studies: boundary integral method

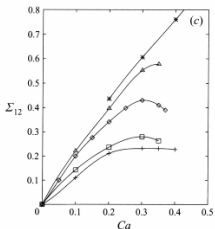
deformation



angle



σ_{xy}



N_1, N_2

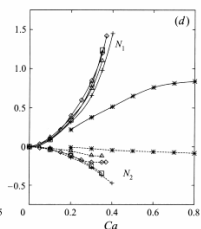


FIGURE 12. Steady-state results as a function of capillary number for $\phi = 10\%$; (a) average steady-state drop deformation, (b) drop orientation, (c) shear stress contribution of drops, and (d) contribution of drops to normal stresses: first normal stress difference (solid curves), second normal stress difference (dashed curves); $\lambda = 0$ (+), $\lambda = 0.2$ (\square), $\lambda = 1$ (\diamond), $\lambda = 2$ (\triangle), $\lambda = 5$ (*).

Different λ . No rupture for $\lambda = 5$ (*)

Flexible thread – deformable microstructure

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Position $\mathbf{x}(s, t)$, arc length s , tension $T(s, t)$

Flexible thread – deformable microstructure

Position $\mathbf{x}(s, t)$, arc length s , tension $T(s, t)$

Slender-body theory with 2:1 drag \perp : \parallel , **S.Ex**

$$\dot{\mathbf{x}} = \mathbf{x} \cdot \nabla \mathbf{U} + T' \mathbf{x}' + \frac{1}{2} T \mathbf{x}''$$

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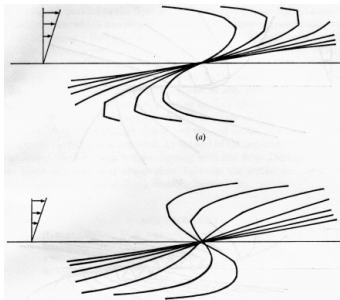
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Snap straight

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- another deformable microstructure

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- ▶ \rightarrow very small change in Einstein $\frac{5}{2}$.

Deformations

- ▶ Emulsions
 - ▶ Rupture
 - ▶ Theories
 - ▶ Numerical
- ▶ Flexible thread
- ▶ Double layer

Microstructural studies for rheology

- ▶ Micro & macro views
- ▶ Einstein viscosity
- ▶ Rotations
- ▶ Deformations
- ▶ Interactions
- ▶ Polymers
- ▶ Others

Interactions

- ▶ Hydrodynamic
 - ▶ Dilute
 - ▶ Experiments
 - ▶ Numerical
- ▶ Electrical double-layer
 - ▶ Concentrated
- ▶ van der Waals
- ▶ Fibres
- ▶ Drops
 - ▶ Numerical

Hydrodynamic interactions for rigid spheres

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Hydrodynamic: difficult long-ranged

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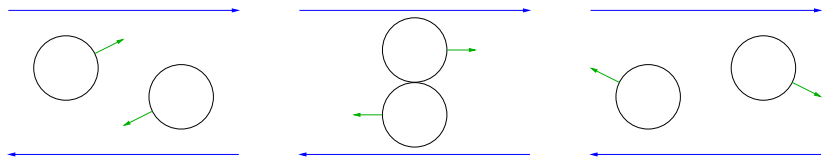
Rigid spheres : two bad ideas

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Dilute – between pairs (mostly)

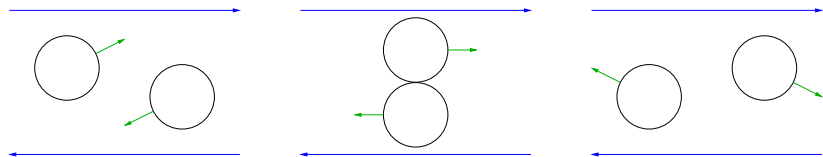


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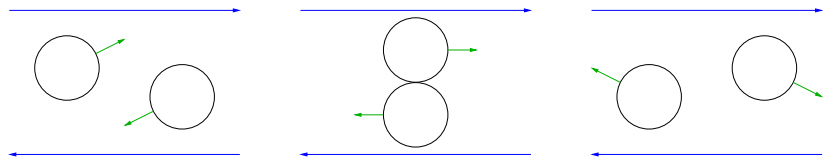
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Reversible (spheres + Stokes flow) \rightarrow return to original streamlines

But minimum separation is $\frac{1}{2} 10^{-4}$ radius \rightarrow sensitive to **roughness** (typically 1%) when do not return to original streamlines.

Summing dilute interactions

Divergent integral from $\nabla \mathbf{u} \sim \frac{1}{r^3}$

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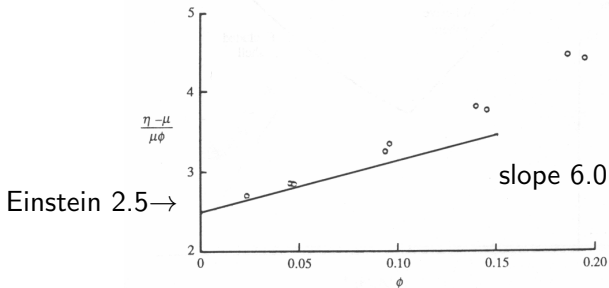
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Small strain-hardening, small shear-thinning

Test of Batchelor ϕ^2 result

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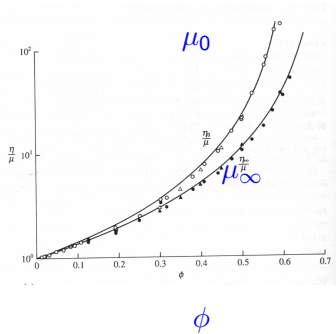
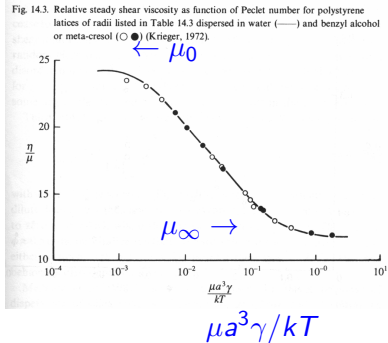
Fig. 14.17. Low shear viscosity for dilute suspensions of hard spheres (Russel, 1980): \circ , data for polystyrene latices ($a=42, 87$ nm) in water (Saunders, 1961); —, theory of Batchelor (1977).



Russel, Saville, Schowalter 1989

Experiments – concentrated

Effective viscosities in shear flow



Russel, Saville, Schowalter 1989

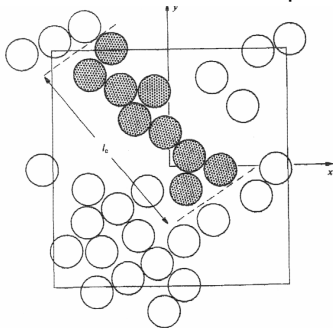
Stokesian Dynamics

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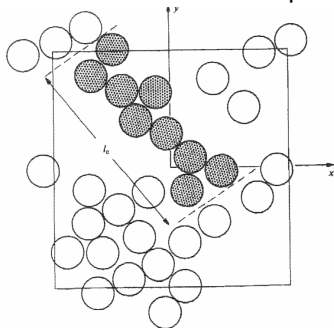


Brady & Bossis (1985)

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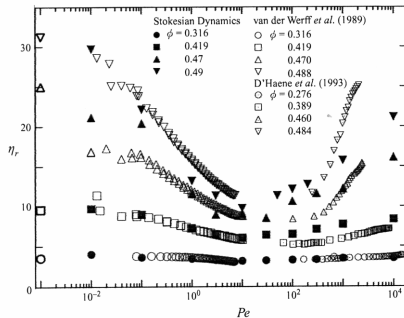


Brady & Bossis (1985)

Fragile clusters if include soft repulsion or Brownian motion

Stokesian Dynamics 2

Effective viscosity in shear flow



Foss & Brady (2000)

'Stokesian Dynamics' Brady & Bossis
Ann. Rev. Fluid Mech. (1988)

Electrical double-layer interactions

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Interaction distance r_* :

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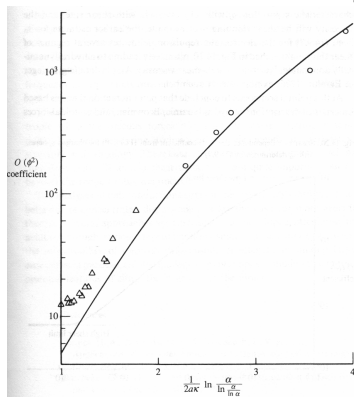
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ϕ^2 coefficient as function of $\frac{r_*}{a}$



Experiments – concentrated

Stress as function of shear-rate at different pH.

Suspension of $0.33\mu\text{m}$ aluminium particles at $\phi = 0.3$

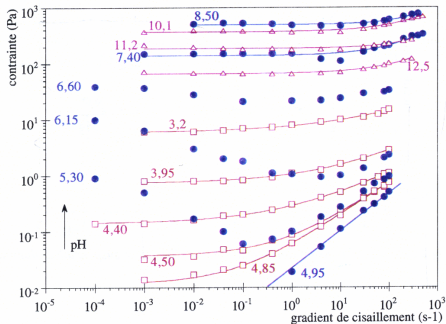


Fig.3 : Courbes d'écoulement de suspensions d'alumine P772SB, en fonction du pH.
 $\phi_v=0,30$.

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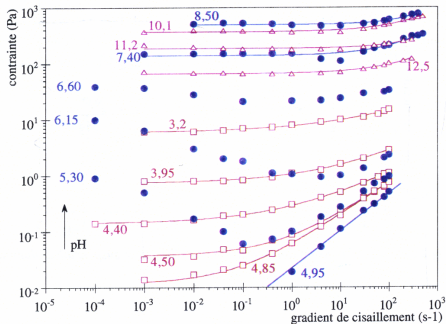


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Breakdown of structure in rheology $\mu(\gamma)$

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Disk not random if $\phi \frac{1}{r} > 1$.

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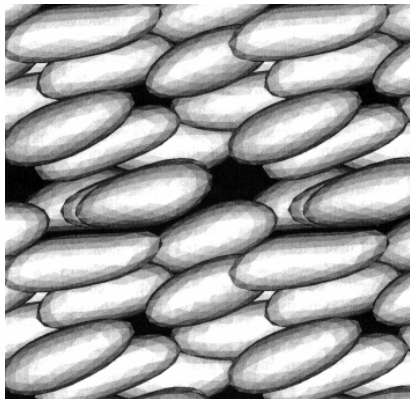
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- ▶ Deformed shape has lower collision cross-section
so 'dilute' at $\phi = 0.3$, **blood works!**

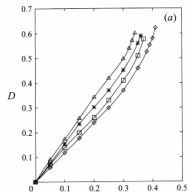
Numerical studies: boundary integral method



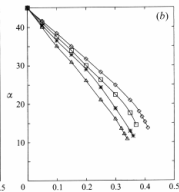
$\phi = 0.3$, $Ca = \mu_{\text{ext}}\gamma a/T = 0.3$ $\lambda = 1$, $\gamma t = 10$,
12 drops, each 320 triangles.

Numerical studies: boundary integral method 3

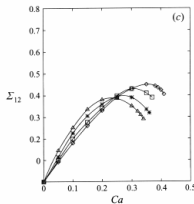
deformation



angle



σ_{xy}



N_1, N_2

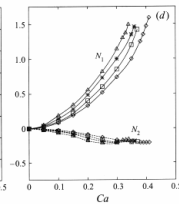
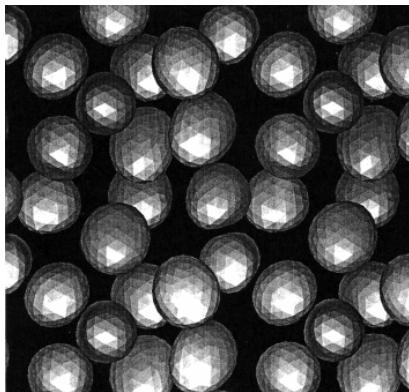


FIGURE 10. Steady-state results as a function of capillary number for $\lambda = 1$. (a) Average steady-state drop deformation, (b) drop orientation, (c) shear stress contribution of drops, and (d) contribution of drops to normal stresses: first normal stress difference (solid curves), second normal stress difference (dashed curves); $\phi = 0$ (\circ), $\phi = 10\%$ (\square), $\phi = 20\%$ ($*$), $\phi = 30\%$ (\triangle).

$\lambda = 1$, different $\phi = 0, 0.1, 0.2, 0.3$. Effectively dilute at $\phi = 0.3$.

Numerical studies: boundary integral method 4

Reduced cross-section for collisions



into flow

Interactions

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