

Instabilities of a thin coating on a vertical fibre; Newtonian, shear-thinning, and elastic liquids

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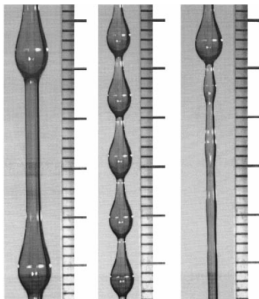
CMS-DAMTP, University of Cambridge

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and Claire McIlroy for elastic liquids

Motivation

Manufacture of polymeric and optical fibres.



Newtonian

Kliakhandler, Davis & Bankoff JFM 2001



Shear-thinning

Duprat, Ruyer-Quil & Giorgiutti-Dauphiné

Phys. Fluids 2009

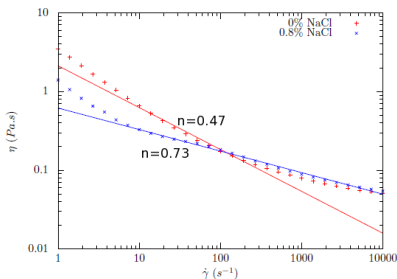
The coating fluid is often non-Newtonian

Governing equations

Constitutive equation

$$\text{Power-law viscosity: } \mu = \beta \left| \frac{\partial u}{\partial y} \right|^{n-1}$$

Xanthan solutions



Boulogne et al, Private Communication

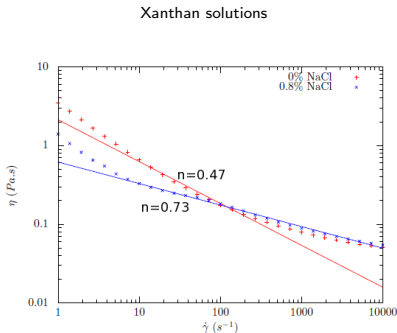
This talk start with power-law, with Newtonian as special case. Elastic at end.

Governing equations

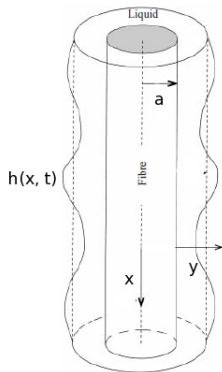
Constitutive equation

Power-law viscosity: $\mu = \beta \left| \frac{\partial u}{\partial y} \right|^{n-1}$

Geometry
Axisymmetric



Boulogne et al, Private Communication



This talk start with power-law, with Newtonian as special case. Elastic at end.

Governing equations

Lubrication framework

Capillary pressure: $p = -\gamma \left(\frac{h}{a^2} + h_{xx} \right)$

Momentum: $0 = -\frac{dp}{dx} + \rho g + \frac{\partial \sigma_{xy}}{\partial y}$

Volume flux: $Q = \beta^{-\frac{1}{n}} \frac{n}{2n+1} \left(\rho g - \frac{dp}{dx} \right)^{\frac{1}{n}} h^{(2+\frac{1}{n})}$

Note: $(\cdot)^{\frac{1}{n}} = \text{sign}(\cdot) \cdot |\cdot|^{\frac{1}{n}}$

Mass conservation: $h_t + Q_x = 0$

Governing equations

Non-dimensionalisation

Lengthscales:

- ▶ Fibre radius, a , in x direction.
- ▶ Initial film thickness, h_0 , in y direction.

Time:

- ▶ Rayleigh instability, $\frac{2n+1}{n} \left(\frac{\beta a^{n+3}}{\gamma h_0^{n+2}} \right)^{\frac{1}{n}}$.

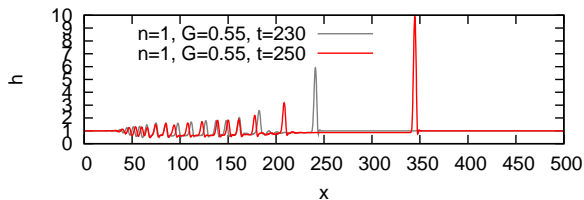
$$h_t + \left(h^{2+\frac{1}{n}} (G + (h + h_{xx})_x)^{\frac{1}{n}} \right)_x = 0$$

where Bond number $G = \frac{\rho g a^3}{\gamma h_0}$.

Time-dependent numerical simulations

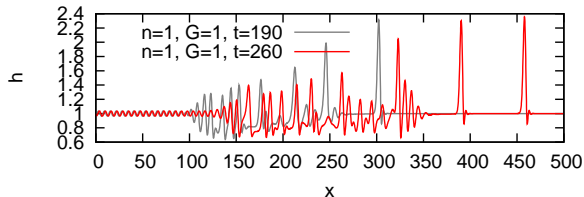
Periodic forcing at inlet: $\omega = 1$

G small (thicker film):



Ever growing
large pulses

G big (thinner film):



Solitary waves
of similar
amplitude and
speed

This talk: Solitary waves? When? Properties?

Stationary solitary waves

Governing equations

In the frame of the solitary waves travelling with speed c :

$$(G + (h + h_{xx})_x) = \frac{\left(c(h - 1) + G^{\frac{1}{n}}\right)^n}{h^{2n+1}}$$

$$h \rightarrow 1, \quad \text{as } x \rightarrow \pm\infty$$

Numerically construct the stationary solitary waves.

- ▶ Integrate from $x = -\infty$ to $x = 0$,
and from $x = +\infty$ to $x = 0$.
- ▶ Hence need starting conditions at $x = \pm\infty$.

Stationary solitary waves

Initial conditions for numerics

At $x = \pm\infty$: $h \sim 1 + \tilde{h}$ with $\tilde{h} \ll 1$.

Linearised equation:

$$\tilde{h}''' + \tilde{h}' - A\tilde{h} = 0$$

where $A = nG^{1-1/n}c - (2n+1)G > 0$.

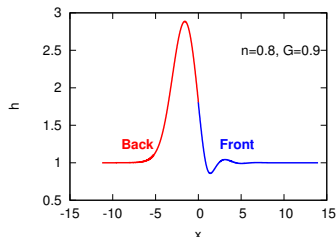
Three solutions of exponential form:

- ▶ $\tilde{h}_1 = a_1 e^{m_1 x}$
 m_1 real and positive: growing mode.

Use in 'Back' (1 DoF).

- ▶ $\tilde{h}_{2,3} = a_{2,3} e^{m_{2,3} x}$
 $m_{2,3}$ complex conjugates with negative real part: decaying modes.

Use in 'Front' (2 DoF).

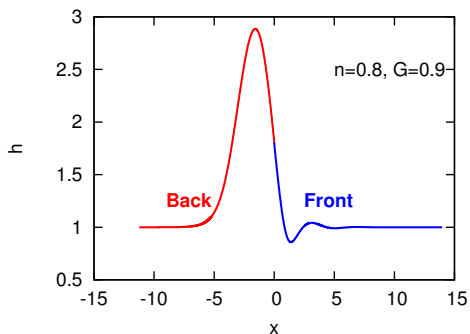


Stationary solitary waves

Numerical construction

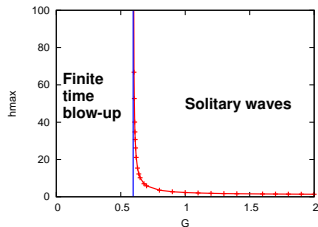
For fixed G :

1. Shoot from **Back**, with $a_2 = a_3 = 0$. Stop when $h'' = 0$, $h' < 0$.
2. Shoot from **Front**, with $a_1 = 0$. Stop when $h'' = 0$, $h' < 0$, $h > 1.5$.
3. Vary the phase of $a_{2,3}$ in **Front** to match h .
4. Vary speed c to match h' .

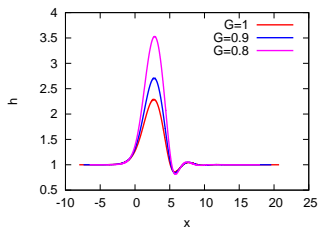


Stationary solitary waves

Results: $n = 1$ Kalliadasis & Chang, J. Fluid Mech. 1994



- ▶ No stationary solitary waves for $G < G_0$.
- ▶ As $G \downarrow G_{0+}$, $h_{\max} \rightarrow \infty$.



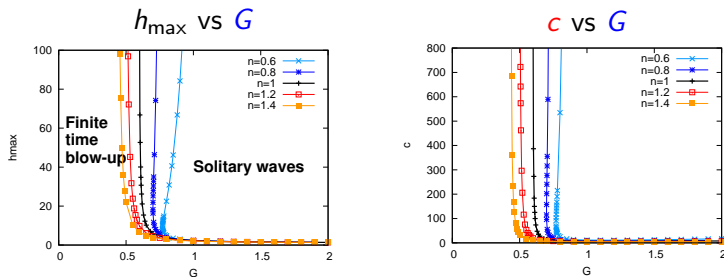
- ▶ Width of the 'Main Body' independent of G .

Agreement with experiment Quéré, Europhys. Lett. 1990:

- ▶ Critical h_c to observe disturbance $\propto a^3$.
- ▶ $G = \frac{\rho g a^3}{\sigma h_0} \Rightarrow h_c \propto a^3$ at $G = G_0$.

Stationary solitary waves

Results: various n (shear-thinning and shear-thickening)



- ▶ Two branches of solutions for $n < 1$.

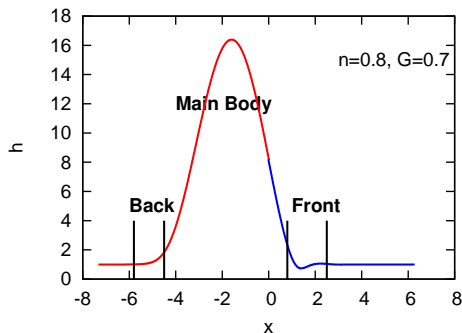
Look at large fast stationary solitary waves close to G_0 .

What determines critical G_0 ? Relationship of h and c with G ?

Large fast solitary waves

Pulse divided into 3 regions:

- ▶ 'Main body' region: h big, $x \sim O(1)$.
- ▶ 'Front' and 'Back' transition regions: $h \sim O(1)$, x small.



Asymptotic analysis for each region, and match. **Very complicated!**

Large fast solitary waves

Main body region: leading order

h big, $x \sim O(1)$

$$(G + (\mathbf{h} + \mathbf{h}_{xx})_x) = \frac{(c(h-1) + G^{\frac{1}{n}})^n}{h^{2n+1}}$$

Solution: constant capillary pressure ($p = \frac{1}{2}h_{\max}$)

$$h = \frac{1}{2}h_{\max}(1 - \cos x) \quad \text{in} \quad 0 \leq x \leq 2\pi.$$

For matching,

$$h \sim \frac{1}{4}h_{\max}(x - x_0)^2,$$

with $x_0 = 0$ at the Back and $x_0 = 2\pi$ at the Front.

At leading order main body is at a constant pressure

Large fast solitary waves

Transition regions: leading order

$h \sim O(1)$, x small

$$(G + (h + \mathbf{h}_{xx})_x) = \frac{\left(c(\mathbf{h} - \mathbf{1}) + G^{\frac{1}{n}}\right)^n}{\mathbf{h}^{2n+1}}$$

Transition regions: $x \sim c^{-n/3}$.

Modified Bretherton equation:

$$h_{\xi\xi\xi} = \frac{(h - 1)^n}{h^{2n+1}} \quad \text{with} \quad \xi = c^{n/3}(x - x_0).$$

($x_0 = 0$ at 'Back' and $x_0 = 2\pi$ at 'Front'.)

Large fast solitary waves

Transition regions: leading order

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($x_0 = 0$ at 'Back' and $x_0 = 2\pi$ at 'Front'.)

For matching, solutions towards 'Main Body' (h becoming large)

$$h \sim \frac{1}{2}P_{\pm}\xi^2 + Q\xi + R_{\pm} \quad \text{as} \quad \xi \rightarrow \pm\infty$$

Use **1 DoF** to redefine origin so $Q = 0$.

Large fast solitary waves

Matching: leading order

DoFs at Back: $1 - 1(Q = 0) = 0$. P_+ and R_+ uniquely determined.

DoFs at Front: $2 - 1(Q = 0) = 1$. One parameter in P_- and R_- .

Main body: $h \sim \frac{1}{4}h_{\max}(x - x_0)^2$ near $x_0 = 0, 2\pi$.

Transition regions: $h \sim \frac{1}{2}P_{\pm}\xi^2 + R_{\pm}$ as $\xi \rightarrow \pm\infty$.

Matching, i.e. same quadratic:

$$P_- = P_+$$

So now P_- unique and hence R_- unique.

$$\frac{1}{2}P(\xi = c^{n/3}(x - x_0))^2 = \frac{1}{4}h_{\max}(x - x_0)^2$$

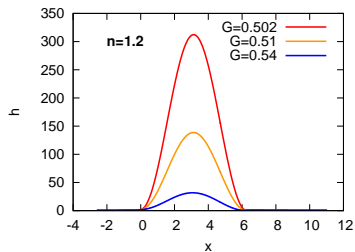
$$h_{\max} = 2Pc^{2n/3}$$

Note: capillary pressure in the main body $p = \frac{1}{2}h_{\max} = Pc^{2n/3}$.

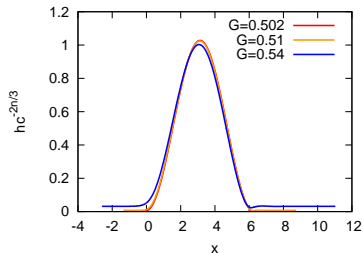
Large fast solitary waves

Checking scalings

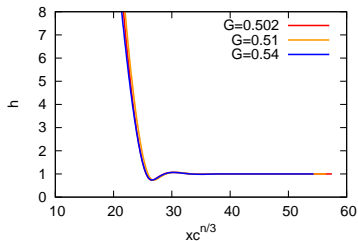
Original profile:



Main body:
height scaled by $c^{-2n/3}$



'Front' transition region:
width scaled by $c^{n/3}$



Large fast solitary waves

So far have $h_{\max}(c)$. G yet to appear

Large fast solitary waves

So far have $h_{\max}(c)$. G yet to appear

Transition regions: $h \sim \frac{1}{2}P\xi^2 + R_{\pm}$.

- ▶ Different apparent film thickness, R_{\pm} , at 'Back' and 'Front'.

Need 1st correction of Main Body: $h \sim c^{2n/3}h_0 + h_2$

$$(G + (h + h_{xx})_x) = \frac{(c(h-1) + G^{1/n})^n}{h^{2n+1}}$$

$$G_0 + (h_2 + h_{2xx})_x = 0$$

Large fast solitary waves

So far have $h_{\max}(c)$. G yet to appear

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$$(G + (h + h_{xx})_x) = \frac{(c(h-1) + G^{1/n})^n}{h^{2n+1}}$$

$$G_0 + (h_2 + h_{2xx})_x = 0$$

Solution (hydrostatic pressure gradient):

$$h_2 = -G_0(x - \sin x) + R_+ \quad \text{in } 0 \leq x \leq 2\pi.$$

Matching gives critical G_0 :

$$G_0 = (R_+ - R_-)/2\pi$$

$2\pi G_0$ pressure difference between pushing and pulling transitions

Large fast solitary waves

c as a function of G

So far have $h_{\max}(c)$ and critical G_0 . Yet to find $G(c)$.

Large fast solitary waves

c as a function of G

So far have $h_{\max}(c)$ and critical G_0 . Yet to find $G(c)$.

Need 2nd correction in Main Body:

$$h \sim c^{2n/3} h_0 + h_2 + c^{-(2n-1)n/3} h_3$$

$$G = G_0 + c^{-(2n-1)n/3} G_1$$

$$(h_3 + h_{3xx})_x = \left(\frac{1}{P^{n+1}(1 - \cos x)^{n+1}} - G_1 \right)$$

Solution

$$P^{n+1} h_3 = \frac{(n+1) \sin x}{n(2n+1)(1 - \cos x)^n} - \frac{(n + (n+1) \cos x) \sin x}{(2n+1)(2n-1)(1 - \cos x)^n} \\ + \frac{(n-1)(n + (n+1) \cos x)}{(2n+1)(2n-1)} \int_{\pi}^x \frac{1}{(1 - \cos t)^{n-1}} dt - G_1 x$$

Large fast solitary waves

c as a function of G

Near $x = x_0$

$$h_3 \sim S(x - x_0)^{1-2n} + D_{\pm} - G_1 x + \dots$$

- ▶ The **singular term** matches the same in transition regions.
- ▶ D_{\pm} different at the 'Back' and 'Front'.
- ▶ No terms to match with them from transition regions.
- ▶ Hence need:

$$G_1 = (D_+ - D_-)/2\pi$$

Finally we have found the relationship between c and G

$$G = G_0 + c^{-(2n-1)n/3} G_1$$

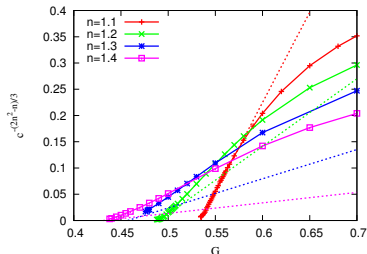
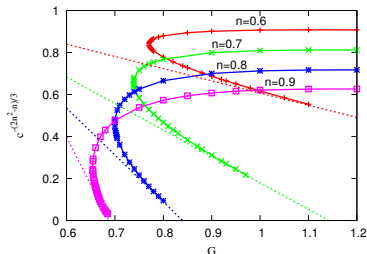
$2\pi G_1$ is the extra pressure difference compared with $n = 1$ to drive flow through main body

Large fast solitary waves

Results

$$G = G_0 + c^{-(2n-1)n/3} G_1$$

Plot $c^{-(2n-1)n/3}$ vs G



- ▶ When $n < 1$, $G_1 < 0$. Negative slope at G_0 .
- ▶ When $n > 1$, $G_1 > 0$. Positive slope at G_0 .
- ▶ When $n = 1$, $G_1 = 0$. No relationship between G and c yet.

More terms

transition regions

With scaling $\xi = c^{n/3}(x - x_0)$,

$$h_{\xi\xi\xi} = \frac{(h-1)^n}{h^{2n+1}} - c^{-2n/3} h_{\xi} - c^{-n} G + c^{-1} \frac{n(h-1)^{n-1} G^{1/n}}{h^{2n+1}} + \dots$$

Expand h as

$$h \sim h_0 + c^{-2n/3} h_2 + c^{-n} h_3 + c^{-1} h_4 + c^{-4n/3} h_5 + \dots$$

$$h_0''' = \frac{(h-1)^n}{h^{2n+1}},$$

$$h_0 \sim \frac{P}{2} \xi^2 + R_{\pm} + Sx^{1-2n}$$

$$h_2''' = \frac{(h_0-1)^{n-1}(-(n+1)h_0 + (2n+1))}{h_0^{2n+2}} h_2 - h_0',$$

$$h_2 \sim -\frac{P}{4!} \xi^4 + \frac{a_{2\pm}}{2} \xi^2 + c_{2\pm} + k_2 \xi^{3-2n}$$

$$h_3''' = \frac{(h_0-1)^{n-1}(-(n+1)h_0 + (2n+1))}{h_0^{2n+2}} h_3 - G_0,$$

$$h_3 \sim -\frac{G_0}{3!} \xi^3 + \frac{a_{3\pm}}{2} \xi^2 + c_{3\pm}$$

$$h_4''' = \frac{(h_0-1)^{n-1}(-(n+1)h_0 + (2n+1))}{h_0^{2n+2}} h_4$$

$$h_4 \sim \frac{1}{2} a_{4\pm} \xi^2 + c_{4\pm}$$

$$+ \frac{n(h_0-1)^{n-1} G_0^{1/n}}{h_0^{2n+1}},$$

More terms

main body

With $h = c^{2n/3}H$,

$$(H + H_{xx})_x = -c^{-2n/3}G + c^{-(2n+1)n/3} \frac{\left(1 - \frac{c^{-2n/3}}{H} + \frac{G^{1/n}(c^{-1-2n/3})}{H}\right)^n}{H^{n+1}}.$$

Expand H as

$$H \sim H_0 + c^{-2n/3}H_2 + c^{-(2n+1)n/3}H_3 + c^{-n}H_4 + c^{-1}H_5 + c^{-4n/3}H_6 + \dots$$

and G as

$$G \sim G_0 + G_1c^{-(2n-1)n/3} + G_2c^{-2n/3} + \dots$$

$$H'_0 + H''_0 = 0,$$

$$H'_2 + H''_2 = -G_0$$

$$H'_3 + H''_3 = -G_1 + \frac{1}{P^{n+1}(1 - \cos x)^{n+1}},$$

$$H'_4 + H''_4 = 0,$$

$$H'_5 + H''_5 = 0,$$

$$H'_6 + H''_6 = -G_2,$$

$$H_0 = P(1 - \cos x)$$

$$H_2 = G_0(\sin x - x) + A_2 + C_2 \cos x$$

$$H_3 \sim Sx^{1-2n} + D_{\pm} - G_1x + k_2x^{3-2n}$$

$$H_4 = A_4 + B_4 \sin x + C_4 \cos x$$

$$H_5 = A_5 + B_5 \sin x + C_5 \cos x$$

$$H_6 = G_2(\sin x - x) + A_6 + B_6 \sin x + C_6 \cos x$$

More terms

Matching: transition regions

Transition regions=

	h_0	h_2	h_3	h_4	h_5	
$c^{\frac{2n}{3}} [$	$\frac{P}{2}x^2$	$-\frac{P}{4!}x^4$			$+\frac{P}{6!}x^6$	$+ \dots]$
$+c^0 [$	R_{\pm}	$+\frac{a_2}{2}x^2$	$-\frac{G_0}{3!}x^3$		$-\frac{a_2}{4!}x^4$	$+ \dots]$
$+c^{-\frac{2n^2}{3} + \frac{n}{3}} [$	Sx^{1-2n}	$+k_2x^{3-2n}$			$+k_3x^{5-2n}$	$+ \dots]$
$+c^{-\frac{n}{3}} [$			$+\frac{a_3}{2}x^2$			$+ \dots]$
$+c^{\frac{2n}{3}-1} [$				$\frac{a_4}{2}x^2$		$+ \dots]$
$+c^{-\frac{2n}{3}} [$		$C_{2\pm}$			$+\frac{a_5}{2}x^2$	$+ \dots]$

More terms

Matching: main body region

Main body=

$$\begin{aligned} & c^{\frac{2n}{3}} \left[\frac{P}{2}x^2 - \frac{P}{4!}x^4 + \frac{P}{6!}x^6 + \dots \right] \\ & + c^0 \left[-G_0x_0 + A_2 + C_2 - \frac{C_2}{2}x^2 - \frac{G_0}{3!}x^3 + \frac{C_2}{4!}x^4 + \dots \right] \\ & + c^{-\frac{2n^2}{3} + \frac{n}{3}} \left[Sx^{1-2n} - G_1x_0 + D_{\pm} + k_2x^{3-2n} + k_3x^{5-2n} + \dots \right] \\ & + c^{-\frac{n}{3}} \left[A_4 + C_4 - \frac{C_4}{2}x^2 + \dots \right] \\ & + c^{\frac{2n}{3}-1} \left[A_5 + C_5 - \frac{C_5}{2}x^2 \right] \\ & + c^{-\frac{2n}{3}} \left[-G_2x_0 + A_6 + C_6 - \frac{C_6}{2}x^2 - \frac{G_2+B_6}{3!}x^3 + \dots \right] \end{aligned}$$

More terms: matching two regions

At c^0 :

$$G_0 = (R_+ - R_-)/2\pi$$

At $c^{-(2n^2-n)/3}$:

$$G_1 = -(D_+ - D_-)/2\pi$$

At c^{-1} :

$$G_2 = (c_{2+} - c_{2-})/2\pi$$

Hence,

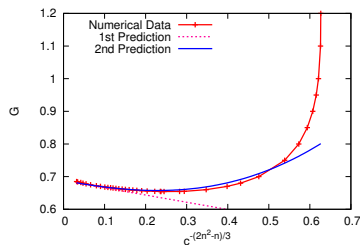
$$G = G_0 + G_1 c^{-(2n-1)n/3} + G_2 c^{-2n/3}$$

More terms: Results

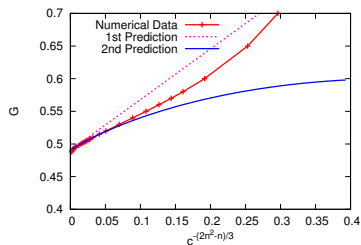
$$G = G_0 + G_1 c^{-(2n-1)n/3} + G_2 c^{-2n/3}$$

Plot G vs $c^{-(2n-1)n/3}$

$n = 0.9$



$n = 1.2$



Small improvement by second correction to G

More terms: Results

$$G = G_0 + G_1 c^{-(2n^2-n)/3} + G_2 c^{-2n/3}$$

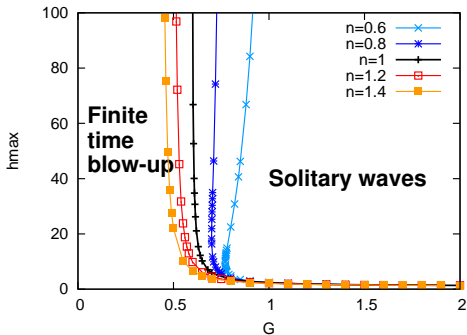
When $n = 1$, $G_1 = 0$, so

$$G = G_0 + G_2 c^{-2/3}$$

Need even more terms for Newtonian $n = 1$ – see beyond end.

$2\pi G_2$ comes from corrections in the transition regions due to the small axial curvature

Two branches for $n < 1$



Upper branch is unstable – solutions either blow up or decay to lower branch.

Hence there is a maximum size of stable solitary for shear-thinning fluids.

Summarising

Main Body at constant pressure $h \sim c^{2n/3} P(1 - \cos x)$.

Cause of all difficulty: length 2π not changing.

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Three mechanisms determine how c depends on $G - G_0$:

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$2\pi G_0$ is extra hydrostatic pressure difference needed to push front transition region compared with pulling rear one.

Three mechanisms determine how c depends on $G - G_0$:

- ▶ For power-law fluids, $G - G_0 \sim G_1 c^{-(2n-1)n/3}$
for pressure to drive flow through main body,
- ▶ For Newtonian ($n = 1$) fluids, $G - G_0 \sim G_2 c^{-2/3}$
effect of axial capillary pressure in the transition regions,
- ▶ For large amplitudes comparable with fibre radius,
 $G - G_0 \sim -\text{amp} c^{-2/3} 3PG_0$
because pendant drop is longer.

Symmetry breaking instability with elastic liquids

with Claire McIlroy

- ▶ François Boulogne observed in his Paris PhD thesis that the coating of an elastic liquid was never axisymmetric, but was always thicker on one side.
- ▶ Flow in thin coating is mainly simple shear and quasi-steady (varies over distances much greater than thickness).
- ▶ Hence rheology is a viscosity plus normal stresses.
- ▶ First normal stress difference = tension in streamlines → enhanced effective surface tension.
- ▶ Second normal stress difference = tension in vortex lines → new instability.

Symmetry breaking instability with elastic liquids

Governing equation

Extra non-Newtonian stress for a second-order fluid

$$\sigma^{NN} = -2\alpha \overset{\nabla}{E} + \beta E^2,$$

α tension in the streamlines, $\beta < 0$ tension in the vortex lines.

$$\frac{\partial h}{\partial t} + G \frac{\partial h^3}{\partial z} + \nabla h^3 \nabla (h + \nabla^2 h) + A \frac{\partial^2}{\partial z^2} h^5 + B \frac{\partial^2}{\partial \theta^2} h^5 = 0,$$

(curiously $A \sim \alpha/6$, but $B \sim -\beta/80$)

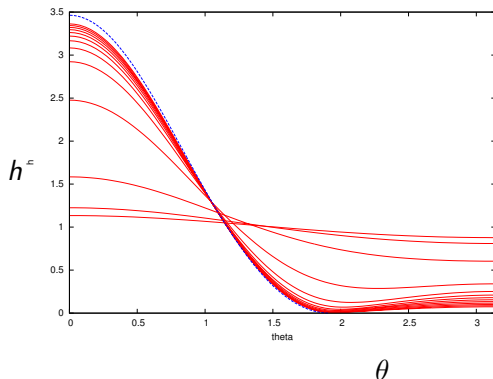
Now study development of lop-sided flow with $h(\theta, t)$,
no z -variations.

$$h_t + (h^3(h_{\theta\theta} + h + B h^2))_{\theta} = 0$$

Symmetry breaking instability with elastic liquids

Time evolution

$h(\theta, t)$ at $t = 2^n$ $n = -2, \dots, 11$, for $B = 0.5$.



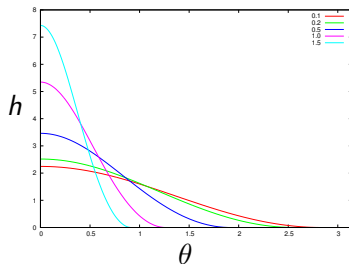
Dotted blue is a steady state which wets only $0 \leq \theta \leq 1.9071$

(Interesting intermediate times: drift of an off-centred cylinder.)

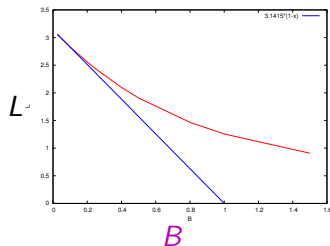
Symmetry breaking instability with elastic liquids

Steady states

Steady states for various B



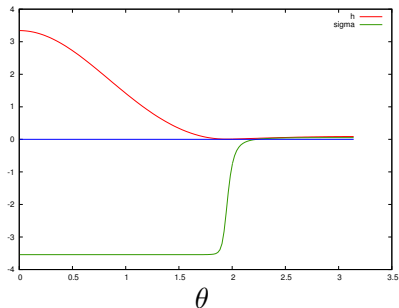
Length of steady state



Symmetry breaking instability with elastic liquids

Structure at late times

The **shape** and the **pressure** (stress $\sigma_{\theta\theta}$) at $t = 10^3$ for $B = 0.5$



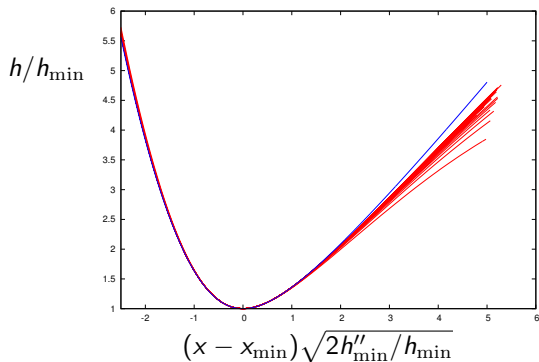
There two constant pressure regions.

Higher pressure region to the right drains into the lower pressure region to the left through a small neck.

Symmetry breaking instability with elastic liquids

The neck between the two constant pressure regions

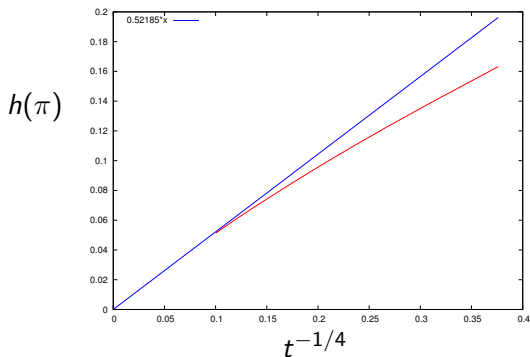
Universal shape of the neck between the two constant pressure regions, for $t = 50$ (50) 10^3 and for $B = 0.5$.



Blue shape from Bretherton's equation.

Symmetry breaking instability with elastic liquids

Draining of small region



$$h(\pi) = \frac{1 + \cos L}{t^{1/4}} \left(\frac{K((\pi - L) \cos L + \sin L)}{4Q \sin^5 L} \right)^{1/4}$$

with Bretherton $Q = 1.20936$ and for $B = 0.5$ pressure in steady state $K = 3.7297$ and length of steady state $L = 1.9171$.

Future Work

- ▶ Normal stress effect. ✓
- ▶ Relax the thin film approximation? ✓
- ▶ Newtonian fluid $n = 1$ ✓
- ▶ What happens at big G ? ✓
- ▶ Finite flow domain for shear-thinning fluids ✓
- ▶ Comparison with experimental data.

$n = 1$ Newtonian fluid, even more terms

Matching: transition regions

Transition regions=

	h_0	h_2	h_3	h_4	
$c^{2/3}$ [$\frac{P}{2}x^2$	$-\frac{P}{4!}x^4$		$+\frac{P}{6!}x^6$	+ ...]
$+c^0$ [R_{\pm}	$+\frac{a_2}{2}x^2$	$-\frac{G_0}{3!}x^3$	$-\frac{a_2}{4!}x^4$	+ ...]
$+c^{-1/3}$ [$-\frac{2}{3P^2x}$		$+\frac{a_3}{2}x^2$	$+\frac{11}{1080P^2}x^3$	+ ...]
$+c^{-2/3}$ [$+c_{2\pm}$		$+\frac{a_4}{2}x^2$	+ ...]
$+c^{-1} \log c$ [$+\frac{4G_0}{9P^3}$		+ ...]
$+c^{-1}$ [$\frac{2(1+2R_{\pm})}{15P^3x^3}$	$+\frac{8R_{\pm}+4+20a_2}{15P^3x}$	$+\frac{4G_0}{3P^3} \log x$	$+c_{3\pm}$	+ ...]

$n = 1$ Newtonian fluid, even more terms

Matching: main body region

Main body =

$$c^{2/3} \left[\frac{P}{2}x^2 - \frac{P}{4!}x^4 + \frac{P}{6!}x^6 + \dots \right]$$

$$+c^0 \left[-G_0x_0 + A_2 + C_2 - \frac{C_2}{2}x^2 - \frac{G_0}{3!}x^3 + \frac{C_2}{4!}x^4 + \dots \right]$$

$$+c^{-1/3} \left[-\frac{2}{3P^2x} + (A_3 + C_3) + \left(\frac{1}{18P^2} + B_3\right)x - \frac{C_3}{2}x^2 + \left(\frac{1}{1080P^2} - \frac{B_3}{3!}\right)x^3 \dots \right]$$

$$+c^{-2/3} \left[-G_2x_0 + A_4 + C_4 + B_4x - \frac{C_4}{2}x^2 - \frac{G_2}{3!}x^3 + \dots \right]$$

$$+c^{-1} \log c \left[A_5 + C_5 - \frac{C_5}{2}x^2 + \dots \right]$$

$$+c^{-1} \left[\frac{2(1+2R_{\pm})}{15P^3x^3} + \frac{4(1+2A_2-3C_2)}{15P^3x} + \frac{4G_0}{3P^3} \log x - G_3x_0 + A_6 + C_6 \dots \right]$$

$n = 1$ Newtonian fluid, even more terms

Results

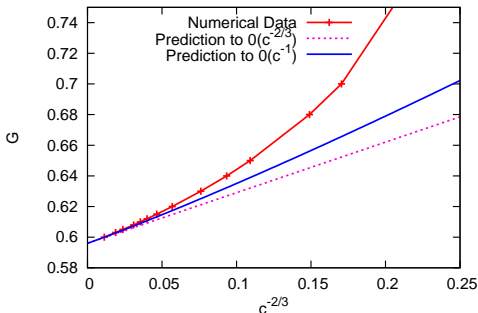
At c^0 : $G_0 = (R_+ - R_-)/2\pi$

At $c^{-2/3}$: $G_2 = (c_{2+} - c_{2-})/2\pi$

At c^{-1} : $G_3 = (c_{3+} - c_{3-})/2\pi$

Hence,

$$G = G_0 + G_2 c^{-2/3} + G_3 c^{-1}$$



$$h \sim 1 + \frac{1}{G} h_1 \quad c \sim \left(2 + \frac{1}{n}\right) G^{\frac{1}{n}} + c_1 G^{\frac{1}{n}-1}$$

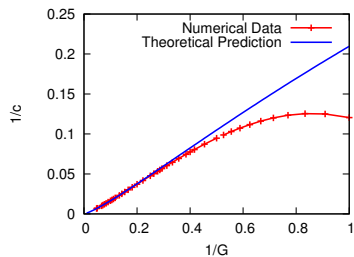
where h_1 satisfies the nonlinear equation

$$h_1' + h_1''' = n c_1 h_1 + h_1^2 \left(-n(2n+1) + \frac{n(n-1)}{2} \left(2 + \frac{1}{n}\right)^2 \right)$$

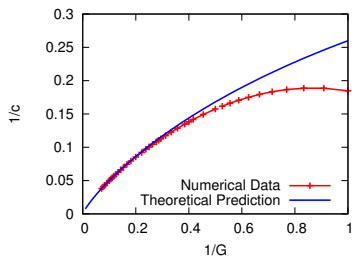
This equation can be solved numerically to give the value of c_1 for different values of n .

Big G results

$n = 0.8$



$n = 1.2$



Finite flow domain for shear-thinning fluids

Modified Bretherton equation

$$h''' = \frac{(h-1)^n}{h^{2n+1}}$$

Integrating from $\pm\infty$ where $h \sim 1 + \tilde{h}$ ($\tilde{h} \ll 1$), \tilde{h} satisfies:

$$\tilde{h}''' = \tilde{h}^n. \Leftarrow \text{No exponential solutions for } n \neq 1.$$

Solution at 'Back'

$$\tilde{h} = A(\xi - \xi_0)^{\frac{3}{1-n}}, \quad n < 1$$

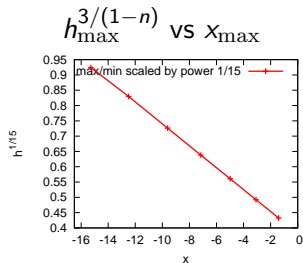
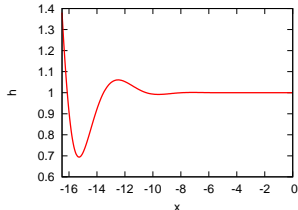
\tilde{h} becomes 0 at a finite distance.

While viscosity thins as $\gamma \rightarrow \infty$ it thickens as $\gamma \rightarrow 0$, and so flow stops in a finite distance.

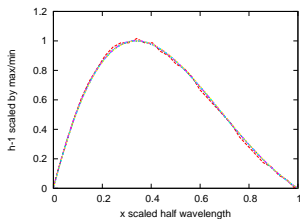
Finite flow domain for shear-thinning fluids

Solution at 'Front' ($n = 0.8$)

Decaying nonlinear oscillations



Each half-cycle normalised by maximum and by wavelength



Universal shape

Decays to zero in finite distance