Birefreingent strand

- thin layer of high stress leaqving a stagnation point
- Wine-glass model of contraction flow
 - anisotropic flow from anisotropic material
- Corner singularity
 - fast flow with no relaxation
- Limited-forec flows
 - strain only to avoid relaxation

$$\frac{DA}{Dt} = A \cdot \nabla \mathbf{u} + \nabla \mathbf{u}^{T} \cdot A - \frac{1}{\tau} (A - \mathbf{I})$$
$$\sigma = -\rho \mathbf{I} + 2\mu_0 E + G \mathbf{f} A$$

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Steady extensional flow



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Steady extensional flow



Microstructure deforms without limit if $E > \frac{1}{2\tau}$: $A = e^{(2E - \frac{1}{\tau})t}$

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Steady extensional flow



Microstructure deforms without limit if $E > \frac{1}{2\tau}$: $A = e^{(2E - \frac{1}{\tau})t}$ Need to limit deformation of microstructure

FENE modification

Finite Extension Nonlinear Elasticity

$$\frac{DA}{Dt} = A \cdot \nabla \mathbf{u} + \nabla \mathbf{u}^T \cdot A - \frac{f}{\tau} (A - \mathbf{I})$$
$$\sigma = -p\mathbf{I} + 2\mu_0 E + GfA$$
$$f = \frac{L^2}{L^2 - \text{trace } A} \quad \text{keeps} \quad A < L^2$$

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Ē

FENE modification

Finite Extension Nonlinear Elasticity



Will use FENE, and if safe Oldroyd-B, in following strong flows

FENE flow past a sphere

Oldroyd-B gave decrease is drag



Chilcott & Rallison 1988 JNNFM

Experiments M1



Tirtaatmadja, Uhlherr & Sridhar 1990 JNNFM

FENE gives drag increase

.... FENE flow past sphere

FENE drag increase from long wake of high stress



Chilcott & Rallison 1988 JNNFM



Cressely & Hocquart 1980 Opt Act

"Birefringent strand"

... birefringent strands

Boundary layers of high stress. Crude model: μ_{ext} in wake, μ_0 elsewhere.



Harlen, Rallison & Chilcott 1990 JNNFM

Can apply to all flows with stagnation points, e.g.



Harlen, Rallison & Chilcott 1990 JNNFM

Also cusps at rear stagnation point of bubbles.





Lubrication flow

$$u(x,y) = U(x)\frac{a-y}{a} + (Q-Ua)\frac{3y(a-y)}{a^2}$$



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Force balance on strand

$$\left[\mu \frac{\partial u}{\partial y}\right]_{0-}^{0+} + \frac{\partial}{\partial x} \left(\frac{\delta \mu_{\text{ext}}}{\partial x}\right)$$



Lubrication flow

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Force balance on strand

$$\left[\mu \frac{\partial \boldsymbol{u}}{\partial \boldsymbol{y}}\right]_{0-}^{0+} + \frac{\partial}{\partial \boldsymbol{x}} \left(\delta \mu_{\text{ext}} \frac{\partial \boldsymbol{U}}{\partial \boldsymbol{x}}\right)$$

Solving (Student Exercise)

$$U(x) = \frac{3Q}{2a} \left(1 - e^{-\sqrt{\frac{8\mu}{\delta\mu_{\rm ext}a}}x} \right)$$

Very low extension rate in the strand can fail to stretch the microstruture, so relax, producing birefringent "pipes".



Harlen, H, Rallison (1992) JNNFM 44

Formation of a cusp at rear stagnation point of a bubble



Rallsion & Malaga (2007) JNNFM 141

FENE contraction flow

Oldroyd-B gave decrease is pressure drop



Szabo, Rallison & Hinch 1997 JNNFM

Cartalos & Piau 1992 JNNFM

FENE gives increase in pressure drop

Increase in pressure drop from long upstream vortex



Szabo, Rallison & Hinch 1997 JNNFM

Experiments



Cartalos & Piau 1992 JNNFM





• Sink flow
$$u = \frac{Q}{2\pi r^2}$$



Bowl:

Sink flow $u = \frac{Q}{2\pi r^2}$ Stretching starts at $\frac{1}{\tau} = E = \frac{\partial u}{\partial r}$, i.e. at $r_E = (Q\tau)^{1/3}$



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- Hence fully stretched only if $De = \frac{Q\tau}{d^3} > L^{3/2}$.



Stem:

• Fully stretched, $A \approx L^2$,



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▶ Fully stretched, $A \approx L^2$, so $\mu_{\text{ext}} = \mu_0 + G\tau L^2 \gg \mu_0 = \mu_{\text{shear}}$



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Szabo, Rallison & H (1997) JNNFM 72

Flow anisotropy from material anisotropy: $\mu_{\mathrm{ext}} \gg \mu_{\mathrm{shear}}$ TDR

If $\nabla \mathbf{u} \gg \frac{1}{\tau}$

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Recall material line elements

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Tensions in streamlines again

Momemtum, ignoring viscous stress

$$0 = -\nabla p + Gg^{1/2}\mathbf{u} \cdot \nabla g^{1/2}\mathbf{u}.$$

Euler equation!!

Momemtum, ignoring viscous stress

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Euler equation!!

Anti-Bernoulli

$$p - \frac{1}{2}Ggu^2 = \text{const}$$



Dollet, Aubouy & Graner 2005 PRL

Potential flows $g^{1/2}\mathbf{u} = \nabla \phi$

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Flow around sharp 270° corner: Hinch 1995 JNNFM

$$\phi = r^{2/3} \cos \frac{2}{3} \theta, \qquad \sigma \propto r^{-2/3} \qquad \psi = r^{14/9} \sin^{7/3} \frac{2}{3} \theta$$

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Alves, Oliviera & Pinho 2003 JNNFM

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Details of the boundary layers - very difficult

Deforming with the flow

While line elements parallel to the flow are stretched $\propto u$, perpendicular elements are squashed $\propto 1/u$, plus some shear.

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While line elements parallel to the flow are stretched $\propto u,$ perpendicular elements are squashed $\propto 1/u,$ plus some shear. Hence try

$$A = \lambda \mathbf{u} \mathbf{u} + \mu (\mathbf{u} \mathbf{v} + \mathbf{v} \mathbf{u}) + \nu \mathbf{v} \mathbf{v}$$

with

$$\mathbf{u} \cdot \mathbf{v} = 0$$
 and $v = 1/u$

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$$\mathbf{u} \cdot \mathbf{v} = 0$$
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Oldroyd-B becomes Student Exercise

$$\mathbf{u} \cdot \nabla \boldsymbol{\lambda} = \frac{2\gamma}{u^2} \mu - \frac{1}{\tau} \left(\boldsymbol{\lambda} - \frac{1}{u^2} \right)$$
$$\mathbf{u} \cdot \nabla \mu = \frac{\gamma}{u^2} \nu \qquad -\frac{1}{\tau} \mu$$
$$\mathbf{u} \cdot \nabla \nu = \qquad -\frac{1}{\tau} \left(\nu - u^2 \right)$$

with

$$\gamma = \mathbf{v} \cdot (\nabla \mathbf{u} + \nabla \mathbf{u}^T) \cdot \mathbf{u} = -u^2 \nabla \cdot \mathbf{v}$$

Renardy (1994) JNNFM 52













Need slow $E = 1/3\tau$ to stop A_{zz} relaxing from χ/Ga

... capillary squeezing

Oldroyd-B
$$a(t) = a(0)e^{-t/3\tau}$$
 does not break

Experiments S1 fluid



Exp: Liang & Mackley 1994 JNNFM

Thy: Entov & Hinch 1997 JNNFM

but filament eventually breaks in experiments

$$\dot{A}_{zz}^{i} = 2\left(\mathbf{E} = -2\frac{\dot{a}}{a}\right)A_{zz}^{i} - \frac{1}{\tau_{i}}A_{zz}^{i}$$

So

$$\dot{A}_{zz}^{i} = 2\left(\boldsymbol{E} = -2\frac{\dot{a}}{a}\right)A_{zz}^{i} - \frac{1}{\tau_{i}}A_{zz}^{i}$$

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Hence momentum equation

$$\frac{\chi}{a} = \frac{1}{a^4} \sum g_i e^{-t/\tau_i}$$

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i 1 $-t/\tau_i$

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Spectrum needed to fit experiments at middle times

FENE capillary squeezing

Filament breaks in with FENE L = 20



Exp: Liang & Mackley 1994 JNNFM

Thy: Entov & Hinch 1997 JNNFM