Chapter 3

Chapter 1: the phenomena.

Chapter 2: measuring intrinsic properties, e.g. viscosity and elasticity.

Chapter 3

Chapter 1: the phenomena.

Chapter 2: measuring intrinsic properties, e.g. viscosity and elasticity.

Now need to encapsulate those properties in governing equations.

Conservation of momentum (Cauchy):

$$\rho \frac{D\mathbf{u}}{Dt} = \nabla \cdot \boldsymbol{\sigma} + \rho \mathbf{g}$$

Conservation of momentum (Cauchy):

$$\rho \frac{D\mathbf{u}}{Dt} = \nabla \cdot \boldsymbol{\sigma} + \rho \mathbf{g}$$

▶ Often inertia (LHS) is negligible.

Conservation of momentum (Cauchy):

$$\rho \frac{D\mathbf{u}}{Dt} = \nabla \cdot \sigma + \rho \mathbf{g}$$

- Often inertia (LHS) is negligible.
- Usually incompressible (plus conservation of mass):

$$\nabla \cdot \mathbf{u} = 0$$

so add pressure to stress, often omitted below.

Conservation of momentum (Cauchy):

$$\rho \frac{D\mathbf{u}}{Dt} = \nabla \cdot \sigma + \rho \mathbf{g}$$

- Often inertia (LHS) is negligible.
- Usually incompressible (plus conservation of mass):

$$\nabla \cdot \mathbf{u} = 0$$

so add pressure to stress, often omitted below.

Need Constitutive (material dependent) Relation between stress σ and flow \mathbf{u} .

Chapter 3

Constitutive equations

Phenomenology

'Simple' materials

Perfectly elastic material

Time derivatives

Exact approximations

Linear viscoelasticity

Second-order fluid

Semi-empirical models

Generalised Newtonian

Oldroyd-B

K-BK7

Lagrangian description

 $\mathbf{X}
ightarrow \mathbf{x}(\mathbf{X},t)$

Lagrangian description

$$X \rightarrow x(X, t)$$

Deformation of line element (for micro-lengths \ll macro-lengths)

$$\delta \mathbf{X} \to \delta \mathbf{x} = A \cdot \delta \mathbf{X}, \qquad A_{iJ} = \frac{\partial x_i}{\partial X_J}$$

A has rotation and stretch, see later.

Lagrangian description

$$X \rightarrow x(X, t)$$

Deformation of line element (for micro-lengths \ll macro-lengths)

$$\delta \mathbf{X} \to \delta \mathbf{x} = A \cdot \delta \mathbf{X}, \qquad A_{iJ} = \frac{\partial x_i}{\partial X_J}$$

A has rotation and stretch, see later.

Local and casual dependency

$$\sigma(t) = \sigma \left\{ A(\tau) \right\}_{\tau \le t}$$

Lagrangian description

$$X \rightarrow x(X, t)$$

Deformation of line element (for micro-lengths \ll macro-lengths)

$$\delta \mathbf{X} \to \delta \mathbf{x} = A \cdot \delta \mathbf{X}, \qquad A_{iJ} = \frac{\partial x_i}{\partial X_J}$$

A has rotation and stretch, see later.

Local and casual dependency

$$\sigma(t) = \sigma \left\{ A(\tau) \right\}_{\tau \le t}$$

This functional dependence not useful,

Lagrangian description

$$X \rightarrow x(X, t)$$

Deformation of line element (for micro-lengths ≪ macro-lengths)

$$\delta \mathbf{X} \to \delta \mathbf{x} = A \cdot \delta \mathbf{X}, \qquad A_{iJ} = \frac{\partial x_i}{\partial X_J}$$

A has rotation and stretch, see later.

Local and casual dependency

$$\sigma(t) = \sigma \left\{ A(\tau) \right\}_{\tau \le t}$$

This functional dependence not useful, except for fast elastic limit and slow viscous limits (each with single parameter)

'Tensorial correct' or result independent of observer,

'Tensorial correct' or result independent of observer, so same stresses if add translation and rotation

$$\mathbf{x}' = \mathbf{a}(t) + Q(t)\mathbf{x}$$

'Tensorial correct' or result independent of observer, so same stresses if add translation and rotation

$$\mathbf{x}' = \mathbf{a}(t) + Q(t)\mathbf{x}$$

so in new frame

$$\sigma' = \sigma \left\{ Q(\tau) A(\tau) Q^{T}(0) \right\}_{\tau \leq t} \equiv Q(t) \sigma \left\{ A(\tau) \right\}_{\tau \leq t} Q^{T}(t).$$

'Tensorial correct' or result independent of observer, so same stresses if add translation and rotation

$$\mathbf{x}' = \mathbf{a}(t) + Q(t)\mathbf{x}$$

so in new frame

$$\sigma' = \sigma \left\{ Q(\tau) A(\tau) Q^{T}(0) \right\}_{\tau \leq t} \equiv Q(t) \sigma \left\{ A(\tau) \right\}_{\tau \leq t} Q^{T}(t).$$

Require $\sigma\{A\}$ to obey this identity for all Q(t).

Instantaneous, no history.

Instantaneous, no history.

Decompose deformation A into first a stretch U followed by a rotation R,

$$A = RU$$
, with $R^T R = I$, by finding A : $U^2 = A^T A$.

Instantaneous, no history.

Decompose deformation A into first a stretch U followed by a rotation R,

$$A = RU$$
, with $R^T R = I$, by finding A : $U^2 = A^T A$.

The set $Q = R^T$ in Material Frame Indifference

$$\sigma\left\{A\right\} = R(t)f(U(t))R^{T}$$

Instantaneous, no history.

Decompose deformation A into first a stretch U followed by a rotation R,

$$A = RU$$
, with $R^T R = I$, by finding A : $U^2 = A^T A$.

The set $Q = R^T$ in Material Frame Indifference

$$\sigma\left\{A\right\} = R(t)f(U(t))R^{T}$$

In incompressible material with isotropic in rest state,

$$f(U^2) = U^2 f_1 + U^{-2} f_2$$
, f_i scalar functions of invariants of U ,

so

$$\sigma = AA^T f_1 + A^{-1} A^{-1} f_2$$

Alternatively for incompressible with isotropic in rest state, use an elastic potential energy w,

Alternatively for incompressible with isotropic in rest state, use an elastic potential energy w,

a function of eigenvalues λ_i of U in invariant combinations

$$\alpha = \frac{1}{2} \left(\lambda_1^2 + \lambda_2^2 + \lambda_3^2 \right), \beta = \frac{1}{2} \left(\lambda_1^{-2} + \lambda_2^{-2} + \lambda_3^{-2} \right), \gamma = \lambda_1 \lambda_2 \lambda_3 \equiv 1$$

Alternatively for incompressible with isotropic in rest state, use an elastic potential energy \boldsymbol{w} ,

a function of eigenvalues λ_i of U in invariant combinations

$$\alpha = \frac{1}{2} (\lambda_1^2 + \lambda_2^2 + \lambda_3^2), \beta = \frac{1}{2} (\lambda_1^{-2} + \lambda_2^{-2} + \lambda_3^{-2}), \gamma = \lambda_1 \lambda_2 \lambda_3 \equiv 1$$

Virtual work and σ co-diagonal with U gives

$$\sigma_1 = \frac{1}{\lambda_2 \lambda_3} \left(\frac{\partial \mathbf{w}}{\partial \lambda_1} = \lambda_1 \frac{\partial \mathbf{w}}{\partial \alpha} - \lambda_1^{-3} \frac{\partial \mathbf{w}}{\partial \beta} \right),$$

Alternatively for incompressible with isotropic in rest state, use an elastic potential energy \boldsymbol{w} ,

a function of eigenvalues λ_i of U in invariant combinations

$$\alpha = \frac{1}{2} \left(\lambda_1^2 + \lambda_2^2 + \lambda_3^2 \right), \beta = \frac{1}{2} \left(\lambda_1^{-2} + \lambda_2^{-2} + \lambda_3^{-2} \right), \gamma = \lambda_1 \lambda_2 \lambda_3 \equiv 1$$

Virtual work and σ co-diagonal with U gives

$$\sigma_1 = \frac{1}{\lambda_2 \lambda_3} \left(\frac{\partial w}{\partial \lambda_1} = \lambda_1 \frac{\partial w}{\partial \alpha} - \lambda_1^{-3} \frac{\partial w}{\partial \beta} \right),$$

SO

$$\sigma = \frac{1}{\gamma} \frac{\partial \mathbf{w}}{\partial \alpha} A A^{T} - \frac{1}{\gamma} \frac{\partial \mathbf{w}}{\partial \beta} A^{-1} A^{-1}.$$

Alternatively for incompressible with isotropic in rest state, use an elastic potential energy \boldsymbol{w} ,

a function of eigenvalues λ_i of U in invariant combinations

$$\alpha = \frac{1}{2} \left(\lambda_1^2 + \lambda_2^2 + \lambda_3^2 \right), \beta = \frac{1}{2} \left(\lambda_1^{-2} + \lambda_2^{-2} + \lambda_3^{-2} \right), \gamma = \lambda_1 \lambda_2 \lambda_3 \equiv 1$$

Virtual work and σ co-diagonal with U gives

$$\sigma_1 = \frac{1}{\lambda_2 \lambda_3} \left(\frac{\partial w}{\partial \lambda_1} = \lambda_1 \frac{\partial w}{\partial \alpha} - \lambda_1^{-3} \frac{\partial w}{\partial \beta} \right),$$

SO

$$\sigma = \frac{1}{\gamma} \frac{\partial w}{\partial \alpha} A A^T - \frac{1}{\gamma} \frac{\partial w}{\partial \beta} A^{-1} A^{-1}.$$

Better for data fitting – Ogden model: $w(\lambda_1^n + \lambda_2^n + \lambda_3^n)$

To express history dependence will use time derivatives and integrals.

To express history dependence will use time derivatives and integrals.

But problem: In new frame

$$\sigma' = Q\sigma Q^T$$

To express history dependence will use time derivatives and integrals.

But problem: In new frame

$$\sigma' = Q\sigma Q^T$$

so its time derivative

$$\dot{\sigma}' = Q\dot{\sigma}Q^T + \dot{Q}\sigma Q^T + Q\sigma\dot{Q}^T$$

To express history dependence will use time derivatives and integrals.

But problem: In new frame

$$\sigma' = Q\sigma Q^T$$

so its time derivative

$$\dot{\sigma}' = Q\dot{\sigma}Q^T + \dot{Q}\sigma Q^T + Q\sigma\dot{Q}^T$$

is different in different frames.

To express history dependence will use time derivatives and integrals.

But problem: In new frame

$$\sigma' = Q\sigma Q^T$$

so its time derivative

$$\dot{\sigma}' = Q\dot{\sigma}Q^T + \dot{Q}\sigma Q^T + Q\sigma\dot{Q}^T$$

is different in different frames.

Now flow transforms

$$u' = Qu + \dot{Q}x + \dot{a}$$

To express history dependence will use time derivatives and integrals.

But problem: In new frame

$$\sigma' = Q\sigma Q^T$$

so its time derivative

$$\dot{\sigma}' = Q\dot{\sigma}Q^T + \dot{Q}\sigma Q^T + Q\sigma\dot{Q}^T$$

is different in different frames.

Now flow transforms

$$u' = Qu + \dot{Q}x + \dot{a}$$

so velocity gradients transform

$$\frac{\partial u'}{\partial x'} = Q \frac{\partial u}{\partial x} Q^T + \dot{Q} Q^T \qquad \text{(watch indices, } \equiv \nabla u^T \text{)}$$

To express history dependence will use time derivatives and integrals.

But problem: In new frame

$$\sigma' = Q\sigma Q^T$$

so its time derivative

$$\dot{\sigma}' = Q\dot{\sigma}Q^T + \dot{Q}\sigma Q^T + Q\sigma\dot{Q}^T$$

is different in different frames.

Now flow transforms

$$u' = Qu + \dot{Q}x + \dot{a}$$

so velocity gradients transform

$$\frac{\partial u'}{\partial x'} = Q \frac{\partial u}{\partial x} Q^T + \dot{Q} Q^T \qquad \text{(watch indices, } \equiv \nabla u^T \text{)}$$

so

strain-rate
$$E' = QEQ^T$$
, vorticity (tensor) $\Omega' = Q\Omega Q^T - \dot{Q}Q^T$

Hence co-rotational (Jaumann) time derivative

$$\overset{\circ}{\sigma} \equiv \frac{D\sigma}{Dt} - \Omega^{T} \cdot \sigma - \sigma \cdot \Omega$$

Hence co-rotational (Jaumann) time derivative

$$\stackrel{\circ}{\sigma} \equiv \frac{D\sigma}{Dt} - \Omega^{\mathsf{T}} \cdot \sigma - \sigma \cdot \Omega$$

has transformation

$$\overset{\circ'}{\sigma'} = Q\overset{\circ}{\sigma}Q^T$$

Student Exercise

Hence co-rotational (Jaumann) time derivative

$$\overset{\circ}{\sigma} \equiv \frac{D\sigma}{Dt} - \Omega^T \cdot \sigma - \sigma \cdot \Omega$$

has transformation

$$\overset{\circ'}{\sigma'} = Q\overset{\circ}{\sigma}Q^T$$

Student Exercise

This is the rate of change of σ seen by an observer rotating with the vorticity, and so is universal.

Hence co-rotational (Jaumann) time derivative

$$\stackrel{\circ}{\sigma} \equiv \frac{D\sigma}{Dt} - \Omega^T \cdot \sigma - \sigma \cdot \Omega$$

has transformation

$$\overset{\circ'}{\sigma'} = Q\overset{\circ}{\sigma}Q^T$$

Student Exercise

This is the rate of change of σ seen by an observer rotating with the vorticity, and so is universal.

Recall rotation frames

$$\overset{\circ}{\mathbf{x}}=\dot{\mathbf{x}}+\Omega\mathbf{x}$$

Can add multiple of $E\sigma + \sigma E$ to co-rotational derivative.

Can add multiple of $E\sigma + \sigma E$ to co-rotational derivative. Hence (upper) co-deformational (Oldroyd-B) derivative

$$\overset{\triangledown}{\sigma} \equiv \frac{D\sigma}{Dt} - \nabla u^T \cdot \sigma - \sigma \cdot \nabla u$$

Can add multiple of $E\sigma + \sigma E$ to co-rotational derivative. Hence (upper) co-deformational (Oldroyd-B) derivative

$$\overset{\triangledown}{\sigma} \equiv \frac{D\sigma}{Dt} - \nabla u^{\mathsf{T}} \cdot \sigma - \sigma \cdot \nabla u$$

has transformation

$$\overset{\triangledown'}{\sigma'} = Q\overset{\triangledown}{\sigma}Q^T$$

Student Exercise

Can add multiple of $E\sigma + \sigma E$ to co-rotational derivative. Hence (upper) co-deformational (Oldroyd-B) derivative

$$\overset{\triangledown}{\sigma} \equiv \frac{D\sigma}{Dt} - \nabla u^{\mathsf{T}} \cdot \sigma - \sigma \cdot \nabla u$$

has transformation

$$\overset{\triangledown'}{\sigma'} = Q\overset{\triangledown}{\sigma}Q^T$$

Student Exercise

Recall stretching material line element

$$\dot{\delta\ell} = \delta\ell \cdot \nabla u$$

Can add multiple of $E\sigma + \sigma E$ to co-rotational derivative. Hence (upper) co-deformational (Oldroyd-B) derivative

$$\overset{\triangledown}{\sigma} \equiv \frac{D\sigma}{Dt} - \nabla u^{\mathsf{T}} \cdot \sigma - \sigma \cdot \nabla u$$

has transformation

$$\overset{\triangledown'}{\sigma'} = Q\overset{\triangledown}{\sigma}Q^T$$

Student Exercise

Recall stretching material line element

$$\dot{\delta\ell} = \delta\ell \cdot \nabla u$$

so for second-order tensor

$$\delta \dot{\ell} \delta \ell = \nabla u^{\mathsf{T}} \cdot \delta \ell \delta \ell + \delta \ell \delta \ell \cdot \nabla u$$

The most general linear response for all materials isotropic in rest state.

The most general linear response for all materials isotropic in rest state.

Linearise in low stretch: $A^T A \approx I$

$$\sigma(t) = R(t) \int_0^\infty \frac{\dot{\sigma}(s) \overline{A^T A}(t-s) ds R^T(t)}{a^T A(t-s)}$$

The most general linear response for all materials isotropic in rest state.

Linearise in low stretch: $A^T A \approx I$

$$\sigma(t) = R(t) \int_0^\infty G(s) \overline{A^T A}(t-s) ds R^T(t)$$

The $R(t) \dots R^{T}(t)$ is a co-rotational integral, but usually dropped in linearisation.

The most general linear response for all materials isotropic in rest state.

Linearise in low stretch: $A^T A \approx I$

$$\sigma(t) = R(t) \int_0^\infty \frac{\dot{\sigma}}{G(s) A^T A} (t-s) \, ds \, R^T(t)$$

The $R(t) \dots R^{T}(t)$ is a co-rotational integral, but usually dropped in linearisation.

Memory kernel G(s) is the Fourier transform of $G^*(\omega)$ of oscillating shear flow.

The most general linear response for all materials isotropic in rest state.

Linearise in low stretch: $A^T A \approx I$

$$\sigma(t) = R(t) \int_0^\infty G(s) \overline{A^T A}(t-s) ds R^T(t)$$

The $R(t) \dots R^{T}(t)$ is a co-rotational integral, but usually dropped in linearisation.

Memory kernel G(s) is the Fourier transform of $G^*(\omega)$ of oscillating shear flow.

For a Newtonian viscous fluid $G(s) = \delta(s)$ and for an elastic solid G(s) = 1.

Student Exercise: If G(t) has a single exponential decay,

$$G(t) = G_0 e^{-t/\tau}$$

show that a polar plot of $Re(G^*)$ versus $Im(G^*)$ as (real) ω varies is part of a circle.

Scalar form for simple shear flow

$$\sigma(t) = \int_0^\infty G(s)\dot{\gamma}(t-s)\,ds$$

Scalar form for simple shear flow

$$\sigma(t) = \int_0^\infty G(s)\dot{\gamma}(t-s)\,ds$$

Hence steady shear viscosity (plug in $\dot{\gamma} = \mathrm{const}$)

$$\mu(0) = \int_0^\infty G(s) \, ds$$

Scalar form for simple shear flow

$$\sigma(t) = \int_0^\infty G(s)\dot{\gamma}(t-s)\,ds$$

Hence steady shear viscosity (plug in $\dot{\gamma}={
m const}$)

$$\mu(0) = \int_0^\infty G(s) \, ds$$

Hence recoil after stop steady shear flow $\dot{\gamma}_0$

$$-\dot{\gamma}_0 \frac{\int_0^\infty sG(s)\,ds}{\int_0^\infty G(s)\,ds}$$

Student Exercise

For weak and slowly varying flows,

For weak and slowly varying flows, the first nonlinear correction

For weak and slowly varying flows, the first nonlinear correction

$$\sigma = -pI + 2\mu E - 2\alpha E + \beta E \cdot E$$

For weak and slowly varying flows, the first nonlinear correction

$$\sigma = -pI + 2\mu E - 2\alpha E + \beta E \cdot E$$

where

$$\mu = \int_0^\infty G(s) ds, \quad \alpha = \int_0^\infty sG(s) ds$$

For weak and slowly varying flows, the first nonlinear correction

$$\sigma = -pI + 2\mu E - 2\alpha E + \beta E \cdot E$$

where

$$\mu = \int_0^\infty G(s) ds, \quad \alpha = \int_0^\infty sG(s) ds$$

from 'retarded motion' expansion.

For weak and slowly varying flows, the first nonlinear correction

$$\sigma = -pI + 2\mu E - 2\alpha E + \beta E \cdot E$$

where

$$\mu = \int_0^\infty G(s) ds, \quad \alpha = \int_0^\infty sG(s) ds$$

from 'retarded motion' expansion.

Hence Cox-Mertz is correct in the limit $\dot{\gamma} \rightarrow$ 0, $\omega \rightarrow$ 0.

For weak and slowly varying flows, the first nonlinear correction

$$\sigma = -pI + 2\mu E - 2\alpha E + \beta E \cdot E$$

where

$$\mu = \int_0^\infty G(s) \, ds, \quad \alpha = \int_0^\infty sG(s) \, ds$$

from 'retarded motion' expansion.

Hence Cox-Mertz is correct in the limit $\dot{\gamma} \rightarrow 0$, $\omega \rightarrow 0$.

Good for dithering Stokes flow, where accumulation of small effects over a long time can produce a significant change.

For weak and slowly varying flows, the first nonlinear correction

$$\sigma = -pI + 2\mu E - 2\alpha E + \beta E \cdot E$$

where

$$\mu = \int_0^\infty G(s) \, ds, \quad \alpha = \int_0^\infty sG(s) \, ds$$

from 'retarded motion' expansion.

Hence Cox-Mertz is correct in the limit $\dot{\gamma} \rightarrow 0$, $\omega \rightarrow 0$.

Good for dithering Stokes flow, where accumulation of small effects over a long time can produce a significant change.

Dangerous in stability analyses and numerical studies, where bad behaviour can occur outside limitation of weak and slowly varying.

Student Exercises

Student Exercises

In simple shear

Student Exercises

In simple shear

ightharpoonup constant viscosity μ

Student Exercises

In simple shear

- ightharpoonup constant viscosity μ
- Normal stress difference $N_1=2\alpha\dot{\gamma}^2$, $N_2=-\frac{1}{4}\beta\dot{\gamma}^2$

Student Exercises

In simple shear

- ightharpoonup constant viscosity μ
- Normal stress difference $N_1=2lpha\dot{\gamma}^2$, $N_2=-rac{1}{4}eta\dot{\gamma}^2$

In (axisymmetric pure) extensional flow

$$\mu_{\text{ext}} = \mu + \left(\alpha + \frac{1}{4}\beta\right)\dot{\epsilon}$$

Student Exercises

In simple shear

- ightharpoonup constant viscosity μ
- Normal stress difference $N_1=2lpha\dot{\gamma}^2$, $N_2=-rac{1}{4}eta\dot{\gamma}^2$

In (axisymmetric pure) extensional flow

- $\mu_{\text{ext}} = \mu + \left(\alpha + \frac{1}{4}\beta\right)\dot{\epsilon}$
- but must keep last term small

Newtonian viscous fluid, except viscosity depends on shear-rate $\dot{\gamma},$

$$\sigma = -pI + 2\mu(\dot{\gamma})E$$
 where $\dot{\gamma} = \sqrt{2E : E}$.

Newtonian viscous fluid, except viscosity depends on shear-rate $\dot{\gamma}$,

$$\sigma = -pI + 2\mu(\dot{\gamma})E$$
 where $\dot{\gamma} = \sqrt{2E : E}$.

Depends on instantaneous flow, i.e. no elastic part and no history.

Newtonian viscous fluid, except viscosity depends on shear-rate $\dot{\gamma}$,

$$\sigma = -pI + 2\mu(\dot{\gamma})E$$
 where $\dot{\gamma} = \sqrt{2E : E}$.

Depends on instantaneous flow, i.e. no elastic part and no history. 'Ad hoc' models to fit experimental data

Newtonian viscous fluid, except viscosity depends on shear-rate $\dot{\gamma}$,

$$\sigma = -pI + 2\mu(\dot{\gamma})E$$
 where $\dot{\gamma} = \sqrt{2E : E}$.

Depends on instantaneous flow, i.e. no elastic part and no history. 'Ad hoc' models to fit experimental data

► Power-law

$$\mu = k\dot{\gamma}^{n-1}$$
, i.e. stress $\sigma \propto \dot{\gamma}^n$

Newtonian viscous fluid, except viscosity depends on shear-rate $\dot{\gamma}$,

$$\sigma = -pI + 2\mu(\dot{\gamma})E$$
 where $\dot{\gamma} = \sqrt{2E : E}$.

Depends on instantaneous flow, i.e. no elastic part and no history. 'Ad hoc' models to fit experimental data

► Power-law

$$\mu = k\dot{\gamma}^{n-1}$$
, i.e. stress $\sigma \propto \dot{\gamma}^n$

► Carreau, Yasuda & Cross

$$\mu = \mu_{\infty} + (\mu_0 - \mu_{\infty}) (1 + (\tau \dot{\gamma})^a)^{(n-1)/a}$$

with plateaux at high and low $\dot{\gamma}.$

More 'ad hoc' models.

More 'ad hoc' models.

Yield fluids which only flow if σ exceeds a yield value σ_Y .

More 'ad hoc' models.

Yield fluids which only flow if σ exceeds a yield value σ_Y .

► Bingham

$$\mu = \begin{cases} \infty, \text{ so } E = 0 & \text{if } \sigma < \sigma_Y \\ \mu_0 + \sigma_Y / \dot{\gamma} & \text{if } \sigma > \sigma_Y \end{cases}$$

Generalised Newtonian

More 'ad hoc' models.

Yield fluids which only flow if σ exceeds a yield value σ_Y .

► Bingham

$$\mu = \begin{cases} \infty, \text{ so } E = 0 & \text{if } \sigma < \sigma_Y \\ \mu_0 + \sigma_Y / \dot{\gamma} & \text{if } \sigma > \sigma_Y \end{cases}$$

► Herchel-Buckley

$$\mu = \begin{cases} \infty, \text{ so } E = 0 & \text{if } \sigma < \sigma_Y \\ \mu_0 \dot{\gamma}^{n-1} + \sigma_Y / \dot{\gamma} & \text{if } \sigma > \sigma_Y \end{cases}$$

 $History\ dependence\ through\ time\ differentials.$

History dependence through time differentials. Easier for computing than with time integrals

History dependence through time differentials. Easier for computing than with time integrals

$$\sigma + \lambda_1 \overset{\triangledown}{\sigma} = 2\mu_0 \left(E + \lambda_2 \overset{\triangledown}{E} \right) \quad \text{with } 0 \leq \lambda_2 \leq \lambda_1.$$

History dependence through time differentials. Easier for computing than with time integrals

$$\sigma + \lambda_1 \overset{\triangledown}{\sigma} = 2\mu_0 \left(E + \lambda_2 \overset{\triangledown}{E} \right) \quad \text{with } 0 \leq \lambda_2 \leq \lambda_1.$$

Three constants

- a viscosity μ₀,
- ightharpoonup a relaxation time λ_1 and
- ightharpoonup a retardation time λ_2 .

History dependence through time differentials. Easier for computing than with time integrals

$$\sigma + \lambda_1 \overset{\triangledown}{\sigma} = 2\mu_0 \left(E + \lambda_2 \overset{\triangledown}{E} \right) \quad \text{with } 0 \leq \lambda_2 \leq \lambda_1.$$

Three constants

- a viscosity μ₀,
- ightharpoonup a relaxation time λ_1 and
- ightharpoonup a retardation time λ_2 .

Special cases

History dependence through time differentials. Easier for computing than with time integrals

$$\sigma + \lambda_1 \overset{\triangledown}{\sigma} = 2\mu_0 \left(E + \lambda_2 \overset{\triangledown}{E} \right) \quad \text{with } 0 \leq \lambda_2 \leq \lambda_1.$$

Three constants

- a viscosity μ₀,
- ightharpoonup a relaxation time λ_1 and
- ightharpoonup a retardation time λ_2 .

Special cases

▶ Maxwell UCM $\lambda_2 = 0$

History dependence through time differentials. Easier for computing than with time integrals

$$\sigma + \lambda_1 \overset{\triangledown}{\sigma} = 2\mu_0 \left(E + \lambda_2 \overset{\triangledown}{E} \right) \quad \text{with } 0 \le \lambda_2 \le \lambda_1.$$

Three constants

- a viscosity μ₀,
- ightharpoonup a relaxation time λ_1 and
- ightharpoonup a retardation time λ_2 .

Special cases

- ▶ Maxwell UCM $\lambda_2 = 0$
- Newtonian $\lambda_1 = \lambda_2$

Student Exercises

Student Exercises

In simple shear

Student Exercises

In simple shear

• constant viscosity $\mu = \mu_0$

Student Exercises

In simple shear

- constant viscosity $\mu = \mu_0$
- Normal stress difference $N_1 = 2\mu_0(\lambda_1 \lambda_2)\dot{\gamma}^2$, $N_2 = 0$

Student Exercises

In simple shear

- constant viscosity $\mu = \mu_0$
- Normal stress difference $N_1=2\mu_0(\lambda_1-\lambda_2)\dot{\gamma}^2$, $N_2=0$

In (axisymmetric pure) extensional flow

Student Exercises

In simple shear

- constant viscosity $\mu = \mu_0$
- Normal stress difference $N_1 = 2\mu_0(\lambda_1 \lambda_2)\dot{\gamma}^2$, $N_2 = 0$

In (axisymmetric pure) extensional flow

$$\mu_{\text{ext}} = \mu_0 \frac{1 - \lambda_2 \dot{\epsilon} - 2\lambda_1 \lambda_2 \dot{\epsilon}^2}{(1 - 2\lambda_1 \dot{\epsilon})(1 + \lambda_1 \epsilon)}$$

Student Exercises

In simple shear

- constant viscosity $\mu = \mu_0$
- Normal stress difference $N_1 = 2\mu_0(\lambda_1 \lambda_2)\dot{\gamma}^2$, $N_2 = 0$

In (axisymmetric pure) extensional flow

•

$$\mu_{\text{ext}} = \mu_0 \frac{1 - \lambda_2 \dot{\epsilon} - 2\lambda_1 \lambda_2 \dot{\epsilon}^2}{(1 - 2\lambda_1 \dot{\epsilon})(1 + \lambda_1 \epsilon)}$$

▶ becomes negative just above $\dot{\epsilon} = 1/2\lambda_1!!!!!$

• White-Metzner to incorporate shear-thinning $\mu(\dot{\gamma})$

$$\sigma + \frac{\mu(\dot{\gamma})}{G} \overset{\triangledown}{\sigma} = 2\mu(\dot{\gamma})E$$

• White-Metzner to incorporate shear-thinning $\mu(\dot{\gamma})$

$$\sigma + \frac{\mu(\dot{\gamma})}{G} \overset{\nabla}{\sigma} = 2\mu(\dot{\gamma})E$$

Giesekus for positive extensional viscosity

$$\sigma + \frac{\alpha \lambda_1}{\mu_0} \sigma^2 + \lambda_1 \overset{\triangledown}{\sigma} = 2\mu_0 E$$

• White-Metzner to incorporate shear-thinning $\mu(\dot{\gamma})$

$$\sigma + \frac{\mu(\dot{\gamma})}{G} \overset{\nabla}{\sigma} = 2\mu(\dot{\gamma})E$$

Giesekus for positive extensional viscosity

$$\sigma + \frac{\alpha \lambda_1}{\mu_0} \sigma^2 + \lambda_1 \overset{\triangledown}{\sigma} = 2\mu_0 E$$

▶ PTT-exponential Phan-Thien & Tanner

$$\sigma + \left[\exp \left(\frac{\lambda_1}{\mu_0} \operatorname{trace} \, \sigma \right) - 1 \right] \sigma + \lambda_1 \overset{\triangledown}{\sigma} = 2\mu_0 E$$

• White-Metzner to incorporate shear-thinning $\mu(\dot{\gamma})$

$$\sigma + \frac{\mu(\dot{\gamma})}{G} \overset{\nabla}{\sigma} = 2\mu(\dot{\gamma})E$$

Giesekus for positive extensional viscosity

$$\sigma + \frac{\alpha \lambda_1}{\mu_0} \sigma^2 + \lambda_1 \overset{\triangledown}{\sigma} = 2\mu_0 E$$

▶ PTT-exponential Phan-Thien & Tanner

$$\sigma + \left[\exp\left(\frac{\lambda_1}{\mu_0} \operatorname{trace} \sigma\right) - 1 \right] \sigma + \lambda_1 \overline{\sigma} = 2\mu_0 E$$

Multi-mode versions of above

Molecular reformulation of Oldroyd-B also for better numerics

Microstructure A:

$$\stackrel{\triangledown}{A} + \frac{f}{\tau}(A - I) = 0$$

Molecular reformulation of Oldroyd-B

also for better numerics

Microstructure *A*:

$$\stackrel{\triangledown}{A} + \frac{f}{\tau}(A - I) = 0$$

Stress σ :

$$\sigma = -pI + 2\mu_0 E + Gf(A - I)$$

Oldroyd-B f = 1

Molecular reformulation of Oldroyd-B

also for better numerics

Microstructure *A*:

$$\overset{\triangledown}{A} + \frac{f}{\tau}(A - I) = 0$$

Stress σ :

$$\sigma = -pI + 2\mu_0 E + Gf(A - I)$$

Oldroyd-B f = 1

FENE modification, for nice behaviour in extensional flow

$$f = \frac{L^2}{L^2 - \text{trace } A}$$

Kay-Bernstein-Kearsley-Zappa

History dependence through time integrals

Kay-Bernstein-Kearsley-Zappa

History dependence through time integrals

Merging of linear viscoelasticity and nonlinear elasticity

$$\sigma = \int_0^\infty \dot{G}(s) \left[\frac{\partial w}{\partial \alpha} \left(\tilde{A} \tilde{A}^T - I \right) - \frac{\partial w}{\partial \beta} \left(\tilde{A}^{-1} \tilde{A}^{-1} - I \right) \right] ds$$

History dependence through time integrals

Merging of linear viscoelasticity and nonlinear elasticity

$$\sigma = \int_0^\infty \dot{G}(s) \left[\frac{\partial w}{\partial \alpha} \left(\tilde{A} \tilde{A}^T - I \right) - \frac{\partial w}{\partial \beta} \left(\tilde{A}^{-1} \tilde{A}^{-1} - I \right) \right] ds$$

where the relative deformation from s to t is

$$\tilde{A} = A(t)A^{-1}(s)$$

History dependence through time integrals

Merging of linear viscoelasticity and nonlinear elasticity

$$\sigma = \int_0^\infty \dot{G}(s) \left[\frac{\partial w}{\partial \alpha} \left(\tilde{A} \tilde{A}^T - I \right) - \frac{\partial w}{\partial \beta} \left(\tilde{A}^{-1} \tilde{A}^{-1} - I \right) \right] ds$$

where the relative deformation from s to t is

$$\tilde{A} = A(t)A^{-1}(s)$$

 $\frac{\partial w}{\partial \alpha}$ and $\frac{\partial w}{\partial \beta}$ are usually replaced by ϕ_1 and ϕ_2 'damping functions',

History dependence through time integrals

Merging of linear viscoelasticity and nonlinear elasticity

$$\sigma = \int_0^\infty \dot{G}(s) \left[\frac{\partial w}{\partial \alpha} \left(\tilde{A} \tilde{A}^T - I \right) - \frac{\partial w}{\partial \beta} \left(\tilde{A}^{-1} \tilde{A}^{-1} - I \right) \right] ds$$

where the relative deformation from s to t is

$$\tilde{A} = A(t)A^{-1}(s)$$

 $\frac{\partial w}{\partial \alpha}$ and $\frac{\partial w}{\partial \beta}$ are usually replaced by ϕ_1 and ϕ_2 'damping functions', not derivatives of some w,

Kay-Bernstein-Kearsley-Zappa

History dependence through time integrals

Merging of linear viscoelasticity and nonlinear elasticity

$$\sigma = \int_0^\infty \dot{G}(s) \left[\frac{\partial w}{\partial \alpha} \left(\tilde{A} \tilde{A}^T - I \right) - \frac{\partial w}{\partial \beta} \left(\tilde{A}^{-1} \tilde{A}^{-1} - I \right) \right] ds$$

where the relative deformation from s to t is

$$\tilde{A} = A(t)A^{-1}(s)$$

 $\frac{\partial w}{\partial \alpha}$ and $\frac{\partial w}{\partial \beta}$ are usually replaced by ϕ_1 and ϕ_2 'damping functions', not derivatives of some w,

functions of combinations α and β eigenvalues of \tilde{A} .

Student Exercises

Student Exercises

In simple shear

Student Exercises

In simple shear

$$\mu = \int_0^\infty \dot{G}(s) (\phi_1 + \phi_2) s \, ds$$
 $N_1 = \int_0^\infty \dot{G}(s) (\phi_1 + \phi_2) s^2 \, ds, \qquad N_2 = -\int_0^\infty \dot{G}(s) \phi_2 s^2 \, ds,$

Student Exercises

In simple shear

$$\mu = \int_0^\infty \dot{G}(s) (\phi_1 + \phi_2) s \, ds$$
 $N_1 = \int_0^\infty \dot{G}(s) (\phi_1 + \phi_2) s^2 \, ds, \qquad N_2 = -\int_0^\infty \dot{G}(s) \phi_2 s^2 \, ds,$

In extensional flow

Student Exercises

In simple shear

$$\mu = \int_0^\infty \dot{G}(s) (\phi_1 + \phi_2) s \, ds$$

$$N_1 = \int_0^\infty \dot{G}(s) (\phi_1 + \phi_2) s^2 \, ds, \qquad N_2 = -\int_0^\infty \dot{G}(s) \phi_2 s^2 \, ds,$$

In extensional flow

$$\mu_{\mathrm{ext}} = \int_{0}^{\infty} \dot{G}(s) \left[\phi_{1} \left(e^{2 \dot{\epsilon} s} - e^{- \dot{\epsilon} s} \right) + \phi_{2} \left(e^{\dot{\epsilon} s} - e^{-2 \dot{\epsilon} s} \right) \right] s \, ds / \dot{\epsilon}$$

Wagner model

$$\phi_2 = 0$$
 so $N_2 = 0$

and

$$\phi_1 = \exp\left(-k\sqrt{\alpha - 3 + \theta(\beta - \alpha)}\right)$$

Wagner model

$$\phi_2 = 0 \quad \text{so } N_2 = 0$$

and

$$\phi_1 = \exp\left(-k\sqrt{\alpha - 3 + \theta(\beta - \alpha)}\right)$$

In shear shear

$$\phi_1 = \exp\left(-k\dot{\gamma}(t-s)\right)$$