

# A Mathieu function boundary spectral method for acoustic scattering

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Example elastic plates produced for Wavinar seminar series:

[https://www.icms.org.uk/V\\_Wavinar.php](https://www.icms.org.uk/V_Wavinar.php)

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With special thanks also to Justin Jaworski (the owl guru) at Lehigh for numerous discussions on the physical models.

# Sketch of talk

**Goal:** Numerically solve scattering problems in applications with complicated BCs. Want: **accurate, fast, flexible** (+ **easy-to-use?**).

Outline (3 fun examples):

- Building a numerical method
- BC I: Porosity (variable Robin)
- Application I: Silent flight of owls
- BC II: Elasticity (4th order coupled ODE)
- Application II: Acoustic black holes
- BC III: Forchheimer (nonlinear inertial correction)
- Application III: Porous foam aerofoils without turbulent simulations
- Conclusions and future work

## Scattering problem

Acoustic 2D scattering governed by the Helmholtz equation

$$\frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} + k_0^2 \phi = 0, \quad (x, y) \in \mathcal{D}.$$

Focus on  $\partial\mathcal{D} = \{(x, 0) : x \in [-1, 1]\}$ .

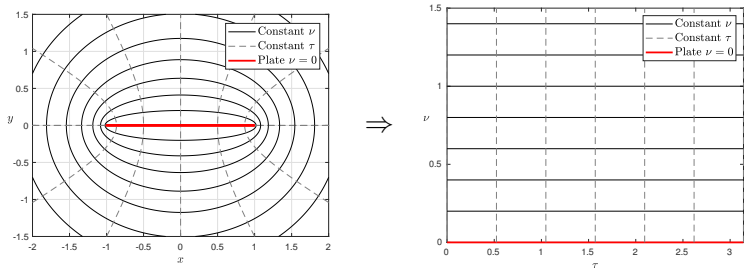
Sommerfeld radiation condition at infinity (radiates to infinity):

$$\lim_{r \rightarrow \infty} r^{\frac{1}{2}} \left( \frac{\partial}{\partial r} - ik_0 \right) \phi(r, \theta) = 0.$$

**NB:** Multiple (non-touching) plates dealt with similarly.

## Simple idea: Separation of variables

Elliptic coordinates  $x = \cosh(\nu) \cos(\tau)$ ,  $y = \sinh(\nu) \sin(\tau)$



$$\phi(\nu, \tau) = \sum_{m=1}^{\infty} a_m s e_m(\tau) H s e_m(\nu).$$

Will determine the unknown coefficients using collocation.

## Angular Mathieu functions

Expand in a rapidly convergent sine series:

$$\text{se}_m(Q; \tau) = \text{se}_m(\tau) = \sum_{l=1}^{\infty} B_l^{(m)} \sin(l\tau), \quad Q = k_0^2/4.$$

For even order solutions, eigenvalue problem becomes

$$\begin{pmatrix} 2^2 - \lambda_{2m} & Q & & & & & \\ Q & 4^2 - \lambda_{2m} & Q & & & & \\ & Q & 6^2 - \lambda_{2m} & Q & & & \\ & & \ddots & \ddots & \ddots & & \\ & & & & & & \end{pmatrix} \begin{pmatrix} B_2^{(2m)} \\ B_4^{(2m)} \\ B_6^{(2m)} \\ \vdots \end{pmatrix} = 0.$$

Similar system for odd order solutions.

## Radial Mathieu functions

Expand in a rapidly convergent Bessel function series:

$$\text{Hse}_m(\nu) = \sum_{l=1}^{\infty} \frac{(-1)^{l+m} B_l^{(m)}}{C_m} \left[ J_{l-1}(e^{-\nu} \sqrt{Q}) H_{l+p_m}^{(1)}(e^{\nu} \sqrt{Q}) \right. \\ \left. - J_{l+p_m}(e^{-\nu} \sqrt{Q}) H_{l-1}^{(1)}(e^{\nu} \sqrt{Q}) \right],$$

where  $p_m = 1$  if  $m$  is even and  $p_m = 0$  if  $m$  is odd.

(Convention:  $C_m$  such that  $\text{Hse}'_m(0) = 1$ .)

**Warning:** Care needed in some regimes to avoid underflow and overflow associated with cancellations between the Bessel and Hankel functions. Solve this using asymptotics (details in C. & Kisil 2020).

**Bottom line:** With a bit of care, both types of Mathieu functions can be accurately and efficiently evaluated  $\Rightarrow$  can be used with collocation.

## Singular integral equation interpretation

Green's function that vanishes on the horizontal axis

$$G(x, y; \tilde{x}, \tilde{y}) = \frac{H_0^{(1)}(k_0 \sqrt{(x - \tilde{x})^2 + (y - \tilde{y})^2}) - H_0^{(1)}(k_0 \sqrt{(x - \tilde{x})^2 + (y + \tilde{y})^2})}{4i}.$$

We get an explicit diagonalisation for  $x \in [-1, 1]$ :

$$\frac{\partial}{\partial y} \int_{-1}^1 \text{se}_m(\cos^{-1}(\tilde{x})) \partial_{\tilde{y}} G(x, 0; \tilde{x}, 0) d\tilde{x} = \frac{d_m}{\sin(\cos^{-1}(x))} \text{se}_m(\cos^{-1}(x)).$$

Examples in this talk can be recast in terms of this double-layer potential.

We can now build a collocation method!



## BC I: Porosity (variable Robin)

Incident field with velocity potential  $\phi_I$ . Impedance BC:

$$\frac{\partial \phi}{\partial y} \Big|_{y=0}(x) + \frac{\partial \phi_I}{\partial y} \Big|_{y=0}(x) = \mu(x)[\phi](x), \quad x \in [-1, 1].$$

Truncate expansion to  $N$  terms, the integral equation becomes

$$\sum_{n=1}^N a_n s e_n(\cos^{-1}(x)) \left[ 1 - 2H s e_n(0) \mu(x) \sqrt{1-x^2} \right] = -\sqrt{1-x^2} \cdot \frac{\partial \phi_I}{\partial y}(x).$$

Collocate at  $N$  Cheb. pts (NB: reformulate as diagonal system if  $\mu=0$ ).

**NB:** Gain sine series for far-field directivity,  $D(\theta)$ , defined via

$$\phi(r, \theta) \sim D(\theta) \frac{e^{iwr}}{\sqrt{r}}, \quad \text{as } r \rightarrow \infty.$$

Total far-field noise, measured in dB:

$$P = 10 \log_{10} \left( \int_0^\pi |D(\theta)|^2 d\theta \right).$$

# Application I: Silent flight of owls

Porosity promotes the silent flight of owls?



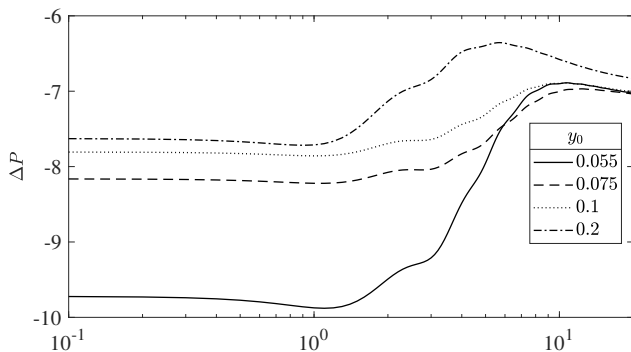
Wing measurements  $\Rightarrow \mu$ .

Owl vs. buzzard in [Ayton, C., Geyer, Chaitanya & Sarradj 2020].

**First study of variable porosity parameter.**

**Goal:** porosity adapted aerofoils for noise reduction

## Application I: Silent flight of owls

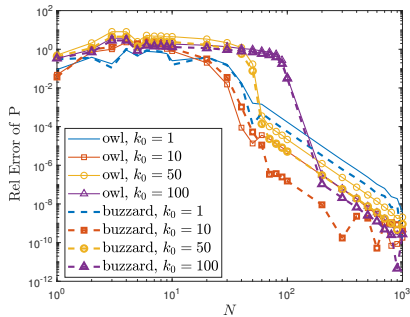
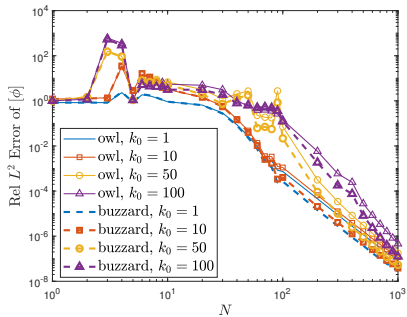


$\Delta P$  for a near-field quadrupole source at  $x_0 = 0.95$  and various  $y_0$ . Negative values indicate the owl is quieter than the buzzard by that many dB.

Further findings:

- Leading-edge noise also reduced for owl (despite similar  $\mu$  there).
- Porosity decreasing from trailing edge to leading edge can be quieter than constant porosity (variably porous plate can induce a destructively interfering leading-edge field)

# Application I: Silent flight of owls



Relative errors for  $[\phi]$  (left,  $L^2$  norm error over  $[-1, 1]$ ) and  $P$  (right).

## BC II: Elasticity (4th order coupled ODE)

Porous plate with evenly-spaced circular apertures of radius  $R$  and fractional open area  $\alpha_H$ . Plate deformation  $\eta(x)$  satisfies:

$$B_0(x)\eta(x) + \sum_{l=1}^4 B_l(x) \frac{\partial^l \eta}{\partial x^l}(x) = -\rho_f c_0^2 \left(1 + \frac{4\alpha_H}{\pi}\right) [\phi](x).$$

Kinematic condition for incident field  $\phi_I$ :

$$\left. \frac{\partial \phi}{\partial y} \right|_{y=0}(x) + \left. \frac{\partial \phi_I}{\partial y} \right|_{y=0}(x) = k_0^2 \left[ (1 - \alpha_H)\eta(x) + \alpha_H \eta_a(x) \right].$$

$\eta_a = 2[\phi]/(\pi k_0^2 R)$  = average fluid displacement in apertures.

Endpoint  $\pm 1$  either free  $\eta'' = \eta''' = 0$  or clamped  $\eta = \eta' = 0$ .

## BC II: Elasticity (4th order coupled ODE)

Expansion of  $\eta$  in Chebyshev polynomials

$$\eta(x) = \sum_{j=0}^{N-1} b_j T_j(x).$$

Collocate thin plate equation at  $N - 4$  Chebyshev points

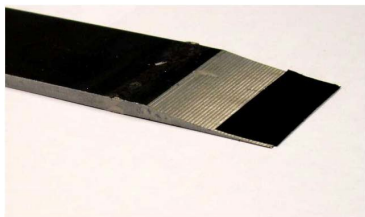
$$\sum_{j=0}^{N-1} \frac{b_j \pi}{2\rho_f c_0^2} \sum_{l=0}^4 B_l(x) T_j^{(l)}(x) + (\pi + 4\alpha_H) \sum_{m=1}^M a_m \text{se}_m(\cos^{-1}(x)) \text{Hse}_m(0) = 0.$$

Collocate kinematic relation at  $M$  Chebyshev points

$$\begin{aligned} \sqrt{1-x^2} \cdot \frac{\partial \phi_I}{\partial y}(x) + \sum_{m=1}^M a_m \text{se}_m(\cos^{-1}(x)) \left[ 1 - \frac{4\alpha_H \text{Hse}_m(0)}{\pi R} \sqrt{1-x^2} \right] \\ = k_0^2 (1 - \alpha_H) \sqrt{1-x^2} \sum_{j=0}^{N-1} b_j T_j(x). \end{aligned}$$

+ 4 relations for  $\eta$  BCs  $\Rightarrow (M + N) \times (M + N)$  system for coefficients.

## Application II: Acoustic black holes



Aluminium plate of thickness  $h(x)$  with

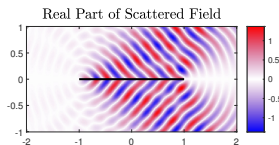
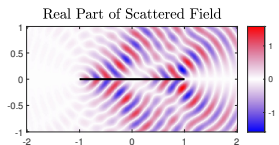
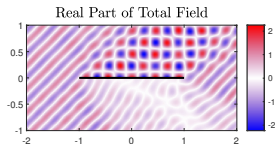
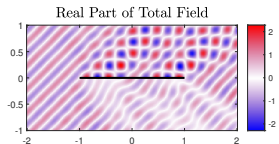
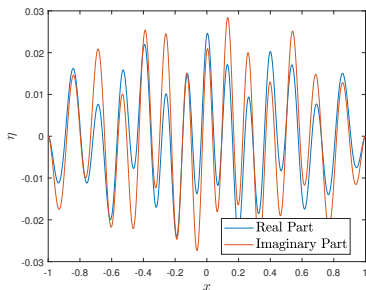
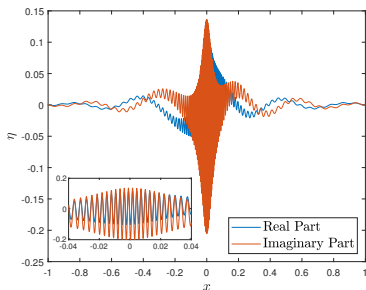
$$B(x) = \frac{Eh(x)^3}{12(1-\nu^2)}, \quad E = 69 \times 10^9 \text{ Pa}, \quad \nu = 0.35$$

$$\frac{d^2}{dx^2} (B(x)\eta''(x)) - m_0 h(x)\eta(x) = -\rho_f c_0^2 \left(1 + \frac{4\alpha_H}{\pi}\right) [\phi](x)$$

**First study of interaction of acoustic blackholes with incident field.**

**Goal:** can acoustic blackholes absorb most of incident field?

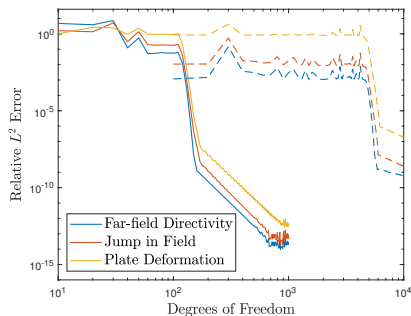
Incident plane wave,  $k_0 = 20$ ,  $h(x) = 0.001x^2 + h_0$



Left:  $h_0 = 10^{-6}$ . Right:  $h_0 = 10^{-3}$ .



# Typical convergence behaviour



Incident plane wave for  $h_0 = 10^{-6}$  (dashed) and  $h_0 = 10^{-3}$  (full).

Several digits of rel. accuracy, even for (nearly) singular elastic BCs!

## BC III: Forchheimer (nonlin. inertial correction for large Re)

$$\frac{\partial \phi}{\partial y} \Big|_{y=0}(x) + \frac{\partial \phi_I}{\partial y} \Big|_{y=0}(x) = C_0(x) \eta_a \Big|_{y=0}, \quad x \in [-1, 1].$$

Nonlinear correction important for foam-like materials:

$$[\phi] = C_1(x) \eta_a + C_2(x) \eta_a |\eta_a|, \quad x \in [-1, 1].$$

$C_1, C_2$  defined in terms of physical parameters. Expand  $\eta_a$  via

$$\eta_a(x) = \sum_{j=0}^{N-1} b_j T_j(x).$$

Collocate nonlinear coupling at  $N$  Chebyshev points

$$2 \sum_{m=1}^M a_m s e_m(\cos^{-1}(x)) \text{Hse}_m(0) = \left[ C_1(x) + C_2(x) \left| \sum_{j=0}^{N-1} b_j T_j(x) \right| \right] \left[ \sum_{j=0}^{N-1} b_j T_j(x) \right].$$

Collocate kinematic relation at  $M$  Chebyshev points

$$\sqrt{1-x^2} \cdot \frac{\partial \phi_I}{\partial y}(x) + \sum_{m=1}^M a_m s e_m(\cos^{-1}(x)) = \sqrt{1-x^2} \cdot C_0(x) \sum_{j=0}^{N-1} b_j T_j(x).$$

## BC III: Forchheimer (nonlin. inertial correction for large $Re$ )

Results in nonlinear system:

$$A\mathbf{v} + (B\mathbf{v}) \circ |C\mathbf{v}| = \mathbf{c}$$

$$A = \left( \begin{array}{c|c} A_{11} & A_{12} \\ \hline A_{21} & A_{22} \end{array} \right), B = \left( \begin{array}{c|c} 0 & 0 \\ \hline 0 & B_{22} \end{array} \right), C = \left( \begin{array}{c|c} 0 & 0 \\ \hline 0 & C_{22} \end{array} \right).$$

Decouple via

$$\mathbf{v}_1 = A_{11}^{-1} (\mathbf{c}_1 - A_{12}\mathbf{v}_2).$$

Solve following via Newton's method:

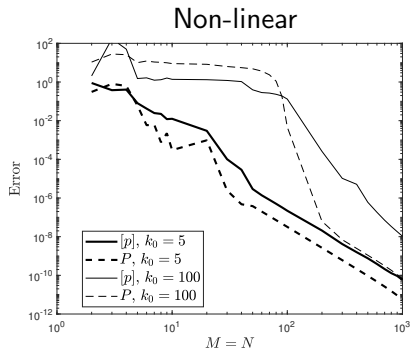
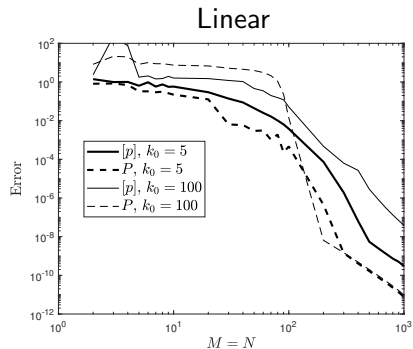
$$[A_{22} - A_{21}A_{11}^{-1}A_{12}] \mathbf{v}_2 + (B_{22}\mathbf{v}_2) \circ |C_{22}\mathbf{v}_2| = -A_{21}A_{11}^{-1}\mathbf{c}_1.$$

In all tested cases:

- $< 10$  iterates needed.
- Initial vector chosen to be solution of linear model.
- Deflation yielded no further solutions.

# Typical convergence behaviour

$$C_0(x) = k_0^2, \quad C_1(x) = ik_0(1.2 + \sin(20x)), \quad C_2(x) = i20k_0^2(x^2 + 1),$$

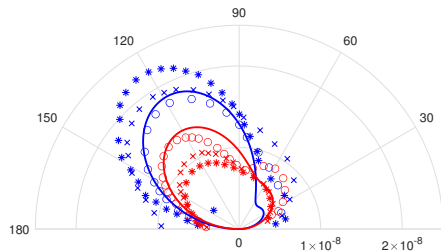


Convergence of the method for the linear case (left) and non-linear case (right).

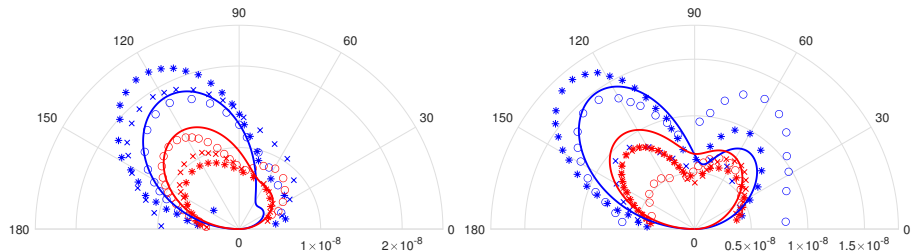
## Application III: Porous foam aerofoils without turbulent sim.

Comparison with Large Eddy Simulations of [Koh et. al. 2018]  
(quadrupole sound source at trailing edge).

$St = 0.3$



$St = 0.4$



Far-field directivity, LES (symbols) and model (solid). Blue corresponds to impermeable/solid, and red to porous. Data computed in less than 0.1s on six year-old laptop

# Concluding Remarks

## Numerical:

- This simple and flexible approach works well in different scenarios and applications (low-mid frequency scattering off  $\lesssim 100$  plates)
- More accurate and faster than basic BEM (comparison in papers).
- Can “diagonalisation” of SIEs be made more general and automatic?
- Can we cope with different domains, e.g. “V” shaped boundaries?
- Can we make it faster (e.g. sparse methods, hierarchical solvers ...) to deal with  $> 100$  scatterers (e.g. model barbules of owl’s wing)?
- How to deal with polylogarithmic singularities more effectively?
- Extension to unbounded plates underway (with A. Hales).

## Physical:

- (I) Porosity *distributions* important due to destructive interferences.
- (II) Acoustic BHs can lead to “transparent” plates and counter-intuitive scattering/sound absorption.
- (III) At mid-high  $k_0$  and high permeability, inertial effects can dominate. Inclusion corrects prev. models’ over-prediction of noise reduction!

# References

## BC/Application I:

- M. Colbrook, M. Priddin. “Fast and spectrally accurate numerical methods for perforated screens.” *IMA Journal of Applied Mathematics*, 2020.
- L. Ayton, M. Colbrook, T. Geyer, P. Chaitanya, E. Sarradj. “Reducing aerofoil–turbulence interaction noise through chordwise-varying porosity” *Journal of Fluid Mechanics*, 2020.

## BC/Application II:

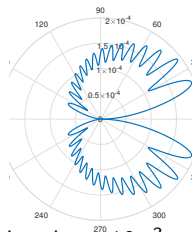
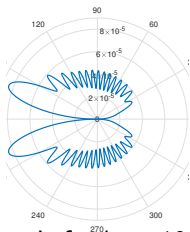
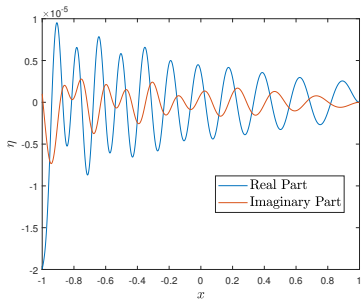
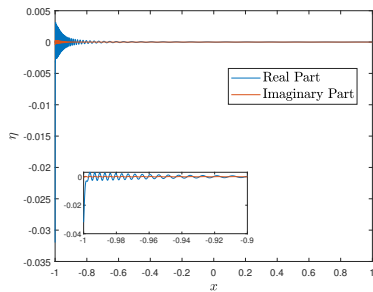
- M. Colbrook, A. Kisil. “A Mathieu function boundary spectral method for scattering by multiple variable poro-elastic plates, with applications to metamaterials and acoustics.” *Proc. Royal Society A*, 2020.

## BC/Application III:

- M. Colbrook, L. Ayton. “Do we need non-linear corrections? – On the boundary Forchheimer equation in acoustic scattering.” *Journal of Sound and Vibration*, under review.

If you have suggestions or problems for collaboration, please get in touch!

Quadrupole at  $(x, y) = (-1, 0.001)$ ,  $k_0 = 25$ ,  $h(x) = 0.001(x + 1)^2 + h_0$



Left:  $h_0 = 10^{-6}$ . Right:  $h_0 = 10^{-3}$ .



## Comparison with BEM

Compare with *Cavalieri, Wolf, & Jaworski, "Numerical solution of acoustic scattering by finite perforated elastic plates", Proceedings A 2016.*

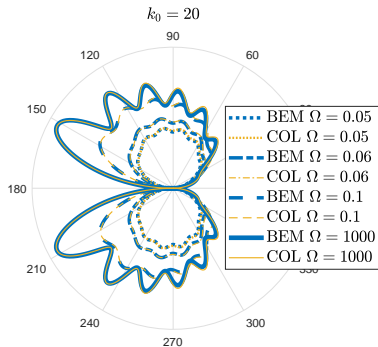
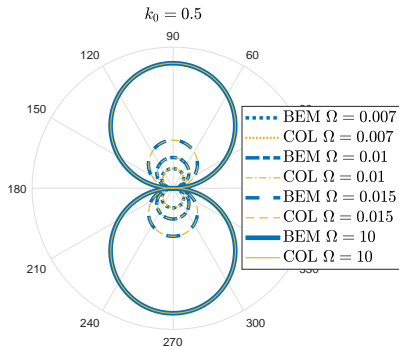
Uses BEM method with basis functions constructed using vibration modes of the plate (computed using standard spectral methods).

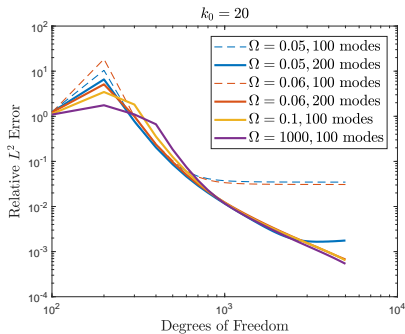
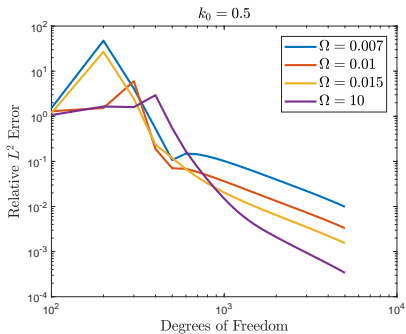
$$(1 - \alpha_H) \frac{\partial^4 \eta}{\partial x^4} - \frac{k_0^4}{\Omega^4} \eta = - \left( 1 + \frac{4\alpha_H}{\pi} \right) \frac{\epsilon}{\Omega^6} k_0^3 [\phi],$$
$$\frac{\partial \phi}{\partial y} \Big|_{y=0} + \frac{\partial \phi_I}{\partial y} \Big|_{y=0} = (1 - \alpha_H) k_0^2 \eta + \frac{2\alpha_H}{\pi R} [\phi].$$

Constant parameters:

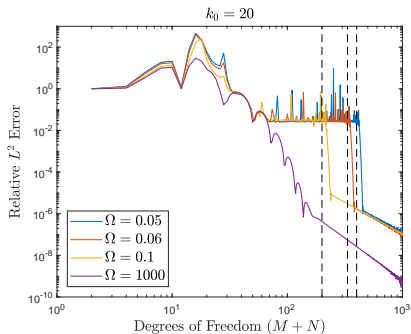
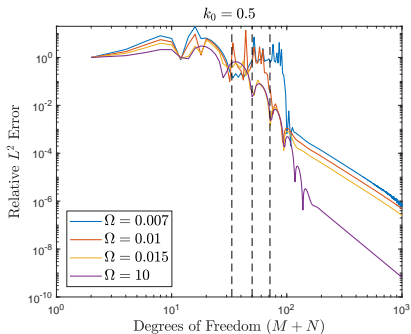
$\Omega$  = vacuum bending wave Mach number

$\epsilon = 0.0021$  = fluid-loading





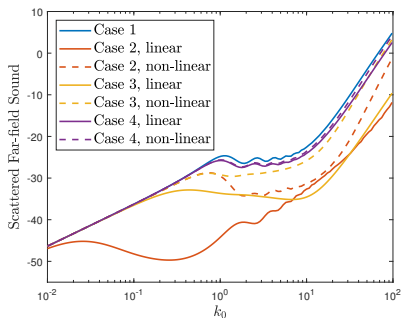
Left: Convergence of elastic BEM for  $k_0 = 0.5$  (100 modes). Right: Same but for  $k_0 = 20$  (number of modes shown).



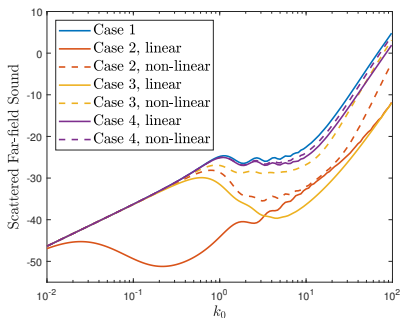
Left: Convergence of Mathieu function collocation for  $k_0 = 0.5$ . The vertical dashed lines are positioned at the bending wavenumbers  $k_B = k_0/\Omega$  (too small to plot for  $\Omega = 10$ ). Right: Same but for  $k_0 = 20$ .

Case	Material	Ref. (see [C. & Ayton 2020])
1	Impermeable	-
2	Alantum NiCrAl open-cell metal foam	[Rubio et. al. 2019]
3	Sintered PE granulate (Porex)	[Geyer et. al. 2014]
4	Sintered SUS316L powder (Group 2, 9mm)	[Zhong et. al. 2018]

Constant  $h$



Variable  $h$



Far-field sound. Left: Results for non-dimensionalised thickness of  $h(x) = 0.012$ . Right: Results for an NACA 4-digit aerofoil.